## DESCRIPTION

Demonstration circuit 1479A is a dual output synchronous buck DC/DC converter featuring the LTC3865EUH. The input voltage range is from 4.5 V to 14 V . The outputs are $1.5 \mathrm{~V} / 15 \mathrm{~A}$ and $1.2 \mathrm{~V} / 15 \mathrm{~A}$. Each output voltage can be precisely programmed to a preset value within $1 \%$ error with the VID pins. The demo board uses a high density, two sided drop-in layout. The package of LTC3865EUH is a small, low thermal impedance $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ 32-Lead QFN.

The light load operation mode of the converter is determined with the MODE/PLLIN pin. Use JP3 jumper to select burst mode, pulse skipping mode or forced continuous mode operation. Switching frequency is pre-set at about 500 KHz . This frequency can be
modified by changing R7 value at the FREQ pin. The converter can also be externally synchronized from 250 kHz to 770 kHz through MODE/PLLIN pin (SYNC terminal on the board). The maximum current sense threshold can be adjusted by connecting $\mathrm{I}_{\text {LIM }}$ pin to SGND, float or INTVcc (with optional R42 and R44). To shut down a channel, force its RUN pin below 1.2V (Jumper: OFF). The power good output (PGOOD terminal) is low when either channel output exceeds $+/-10 \%$ regulation window.

Design files for this circuit board are available. Call the LTC factory.

Table 1. Performance Summary $\left(\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}\right)$

| PARAMETER | CONDITION | VALUE |
| :---: | :---: | :---: |
| Input Voltage Range |  | 4.5 V to 14 V |
| Output Voltage, V $\mathrm{V}_{\text {OT1 }}$ | $\mathrm{V}_{\text {IN }}=4.5-14 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=0 \mathrm{~A}$ to 15 A | $1.5 \mathrm{~V} \pm 1 \% \quad$ (Note) |
| Output Voltage, $\mathrm{V}_{\text {OUT2 }}$ | $\mathrm{V}_{\text {IN }}=4.5-14 \mathrm{~V}, \mathrm{I}_{\text {OUT2 }}=0 \mathrm{~A}$ to 15 A | $1.2 \mathrm{~V} \pm 1 \% \quad$ (Note) |
| Maximum Output Current, Iout1 | $\mathrm{V}_{\text {IN }}=4.5-14 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 1}=1.5 \mathrm{~V}$ | 15A |
| Maximum Output Current, Iout2 | $\mathrm{V}_{\text {IN }}=4.5-14 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 2}=1.2 \mathrm{~V}$ | 15A |
| Typical full load Efficiency, channel 1 | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {OUT } 1}=1.5 \mathrm{~V}, \mathrm{I}_{\text {OUT } 1}=15 \mathrm{~A}$ | 85\% |
| Typical full load Efficiency, channel 2 | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {OUT2 }}=1.2 \mathrm{~V}, \mathrm{I}_{\text {OUT } 2}=15 \mathrm{~A}$ | 83.4\% |
| Typical Switching Frequency |  | 500kHz |

Note: $\mathrm{V}_{\text {OUT1 }}, \mathrm{V}_{\text {OUT2 }}$ are measured directly on output capacitors Cout1 and Cout4.

## QUICK START PROCEDURE

Demonstration circuit 1479A is easy to set up to evaluate the performance of the LTC3865EUH. Refer to Figure 1 for the proper measurement equipment setup and follow the procedure below:

Jumper positions:
JP1,2 (RUN1/RUN2): ON
JP3 (MODE): CCM

1. With power off, connect the input power supply to $\mathrm{Vin}(4.5 \mathrm{~V}-14 \mathrm{~V})$ and GND (input return).
2. Connect the load \#1 between Vout1 and GND (Initial load: no load); connect the load \#2 between Vout2 and GND (Initial load: no load).
3. Connect the DVMs to the input and outputs.
4. Turn on the input power supply and check for the proper output voltages. With current VID pin setting, Vout1 should be $1.5 \mathrm{~V}+/-1 \%$; Vout2 should be $1.2 \mathrm{~V}+/-1 \%$.
5. Once the proper output voltages are established, adjust the loads within the operating range and observe the output voltage regulation, ripple voltage and other parameters.
6. If necessary, change the resistor options on VID pins for another output voltage according to table 2.

Note: 1. When measuring the output or input voltage ripple, do not use the long ground lead on the oscilloscope probe. See Figure 2 for the proper scope probe technique. Short, stiff leads need to be soldered to the $(+)$ and $(-)$ terminals of an output capacitor. The probe's ground ring needs to touch
the (-) lead and the probe tip needs to touch the ( + ) lead.

Note: 2. Do not apply load from Vo1+ to Vo1- or from Vo2+ to Vo2- turrets. These are only intended to conveniently measure the output voltage. Heavy load currents may damage the sense traces.

To accurately measure the output voltages and efficiency, please directly measure Vout1 and Vout2 on output capacitors Cout1 and Cout4.

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## OUTPUT VOLTAGE PROGRAMmING

The output voltages of both channels can be programmed to preset values. There are two VID pins for
each channel: VID11, VID12 for Vout1, and VID21, VID22 for Vout2. See Table 2 for details.

Table 2. Output voltage programming

| VID11/VID21 | VID12NID22 | VOUT1NOUT2 (V) |
| :---: | :---: | :---: |
| INTVCC | INTVCC | $5.0($ Vin > 5V |
| INTVCC | FLOAT | 3.3 |
| INTVCC | GND | 2.5 |
| FLOAT | INTVCC | 1.8 |
| FLOAT | FLOAT | 0.6 or external divider |
| FLOAT | GND | 1.5 |
| GND | INTVCC | 1.2 |
| GND | FLOAT | 1.0 |
| GND | GND | 1.1 |

## SINGLE OUTPUT / DUAL PHASE OPERATION

A single output / dual phase converter may be preferred for high output current applications. The benefits of single output / dual phase operation are lower ripple current through the input and output capacitors, improved load step response and simplified thermal design. To implement single output / dual phase operation, make the following modifications:

1. Tie VOUT1 to VOUT2. Use a piece of heavy copper foil if possible.
2. Tie ITH1 to ITH2 by stuffing $0 \Omega$ at R49.
3. Tie VFB1 to VFB2 by stuffing $0 \Omega$ at R50.
4. Tie TRK/SS1 to TRK/SS2 by stuffing $0 \Omega$ at R52.
5. Tie RUN1 to RUN2 by stuffing $0 \Omega$ at R55.
6. Remove channel 2 ITH compensation network (C44, R35) and float VID21, VID22 pins.

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## RAIL TRACKING

Demonstration circuit 1479A is configured for independent turn-on of VOUT1 and VOUT2. The ramp-rate for VOUT1 is determined by the TRK/SS1 cap at C2 and the ramp-rate for VOUT2 is determined by the TRK/SS2 cap at C47. This board can be modified on the bench to allow VOUT1 to track an external signal.

It can also be modified to allow VOUT2 to track VOUT1 or to allow VOUT2 to track an external signal. Tables 3 and 4 cover the rail tracking options for each rail.

Table 3. VOUT1 Tracking Options (1.5V)

|  | TRACK1 DIVIDER |  | TRK/SS1 CAP |
| :--- | :--- | :--- | :--- |
| CONFIGURATION | R3 | R2 | C2 |
| Soff Start Without Tracking (original board) | $0 \Omega$ | Not stuffed | 0.1 uF |
| External Coincident Tracking | $17.8 \mathrm{k} \Omega$ | $20.0 \mathrm{k} \Omega$ | Not Stuffed |

Table 4. VOUT2 Tracking Options (1.2V)

|  |  | TRACK2 DIVIDER |  |  |
| :--- | :--- | :--- | :--- | :--- |
| CONFIGURATION | R36 | R34 | R37/SS2 CAP |  |
| Soft Start Without Tracking (original board) | $0 \Omega$ | Not stuffed | Not stuffed | C47 |
| Coincident Tracking to VoUT1 (1.5V) | $0 \Omega$ | $10.0 \mathrm{k} \Omega$ | $20.0 \mathrm{k} \Omega$ | Not Stuffed |
| External Coincident Tracking | $10.0 \mathrm{k} \Omega$ | Not stuffed | $20.0 \mathrm{k} \Omega$ | Not Stuffed |

## InDUCTOR DCß SEnSING

Demonstration circuit 1479A provides an optional circuit for DCR sensing. DCR sensing uses the DCR of the inductor to sense the inductor current instead of discrete sense resistors. The advantages of DCR sensing are lower cost, reduced board space and higher efficiency, but the disadvantage is a less accurate current limit. If DCR sensing is used, be sure to select an inductor current with a sufficiently high saturation current or use an iron powder type. Tables 5 and 6 show an example of how to modify the DC1479A for DCR sensing using these parameters:
$V_{\text {OUT1 }}=1.5 \mathrm{~V} / 15 \mathrm{~A}$
$V_{\text {OUT2 }}=1.2 \mathrm{~V} / 15 \mathrm{~A}$
$V_{I N}=4.5 \mathrm{~V}$ to 14 V
Fsw $=500 \mathrm{kHz}$, typical
L1,2 = Vishay IHLP-4040DZERR47M11
( $0.47 \mathrm{uH}, \mathrm{DCR}=1.53 \mathrm{~m} \Omega$ typ, $1.68 \mathrm{~m} \Omega$ max) ILIM = FLOATING (R42,R44 = OPEN)

Table 5. Vout1 Configured as a $1.5 \mathrm{~V} / 15 \mathrm{~A}$ Converter Using DCR Sensing or a Discrete Sense Resistor

|  |  |  | RSENSE FILTER RESISTORS | SENSE <br> FIILTER CAP | DCR FILTER/DIVIDER RESISTORS |  | SENSE1- TO L1JUMPER |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | TOP |  | BOTTOM |  |
| CONFIGURATION | RS1 | L1 |  | R29,R30 | C14 | R45 | R47 | R61 |
| DCR Sensing | Short with Cu strip or very short \& thick piece of wire | $\begin{aligned} & \text { IHLP- } \\ & \text { 4040DZERR47M11 } \end{aligned}$ | Open | 0.22uF | $1.40 \mathrm{k} \Omega$ | $15.4 \mathrm{k} \Omega$ | $0 \Omega$ |
| Discrete RSENSE (original board) | $2 \mathrm{~m} \Omega$ | $\begin{aligned} & \text { IHLP- } \\ & \text { 4040DZERR47M11 } \end{aligned}$ | $100 \Omega$ | 1nF | Open | Open | Open |

Table 6. VOUT2 Configured as a $1.2 \mathrm{~V} / 15 \mathrm{~A}$ Converter Using DCR Sensing or a Discrete Sense Resistor


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Figure 1. Proper Measurement Equipment Setup


Figure 2. Measuring Output Voltage Ripple

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Figure 3. Efficiency vs load current (Vin=12V, 500kHz, CCM)



