Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800

## Products contained in this shipment may be subject to ITAR regulations.

## Warning:

The export of these commodity(ies), technology, or software are subject either to the U.S. Commerce Department Export Administration Regulations (E.A.R.), or to the U.S. State Department International Traffic In Arms Regulations (I.T.A.R.). Diversion, the shipment to unauthorized locations or entities, or the disclosure of related technical data or software to unauthorized foreign nationals is contrary to U.S. law and is prohibited. If export is authorized to a specific country or end-users, compliance with the U.S. export laws is required prior to transfer, transshipment on a non-continuous voyage, or disposal in any other country, or to any other end-user of these commodities, either in their original form or after being incorporated into other end-items.

# Total lonizing Dose (TID) Radiation Testing of the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier for Linear Technology 

Customer: Linear Technology, PO\# 74026L
RAD Job Number: 15-0704
Part Type Tested: RH1056AMW Precision, High Speed, JFET Input Operational Amplifier, Linear Technology RH1056A Datasheet ID No. 66-10-0160 Rev C
Traceability Information: Fab Lot Number: 10217302.1, Lot Number: 780000.1, Wafer Number: 13, Date Code: 1443A. See photograph of unit under test in Appendix A.
Quantity of Units: 11 units received, 5 units for biased irradiation, 5 units for unbiased irradiation and 1 unit for control. Serial numbers 1317, 1318, 1321, 1322 and 1323 were biased during irradiation, serial numbers $1324,1325,1326,1327$ and 1328 were unbiased during irradiation and serial number 1329 was used as control. See Appendix B for the radiation bias connection table.

Radiation and Electrical Test Increments: 50rad(Si)/s ionizing radiation with electrical test increments: pre-irradiation, $10 \mathrm{krad}(\mathrm{Si}), 20 \mathrm{krad}(\mathrm{Si}), 30 \mathrm{krad}(\mathrm{Si}), 50 \mathrm{krad}(\mathrm{Si})$ and $100 \mathrm{krad}(\mathrm{Si})$.
Pre-Irradiation Burn-In: Burn-In performed by Linear Technology prior to receipt by RAD
Overtest and Post-Irradiation Anneal: No overtest. No anneal
Radiation Test Standard: MIL-STD-883 TM1019 Condition A and Linear Technology RH1056A Datasheet ID No. 66-10-0160 Rev C.

Test Hardware and Software: LTS2020 Automated Tester, Entity ID TS04, Calibration Date: 5/28/2015, Calibration Due: 5/28/2016. LTS2101 Family Board, Entity ID FB02. LTS0607 Test Fixture, Entity ID TF41. BGSS-991003 RH1056 DUT Board. Test Program: RH1056LT.SRC
Facility and Radiation Source: Aeroflex RAD's, Colorado Springs, CO. Gamma rays provided by JLSA 81-24 Co60 source. Dosimetry performed by Air Ionization Chamber (AIC) traceable to NIST. Aeroflex RAD's dosimetry has been audited by DLA and Aeroflex RAD has been awarded Laboratory Suitability for MIL-STD-750 and MIL-STD-883 TM 1019.
Irradiation and Test Temperature: Room temperature controlled to $24^{\circ} \mathrm{C} \pm 6^{\circ} \mathrm{C}$ per MIL-STD-883.

High Dose Rate Test Result: PASSED the total ionizing dose test to the maximum tested dose level of $100 \mathrm{krad}(\mathrm{Si})$ with all parameters remaining within their datasheet specifications. Further the units do not exhibit ELDRS as defined in the current test method.

## TID Report 15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800

### 1.0. Overview and Background

It is well known that total dose ionizing radiation can cause parametric degradation and ultimately functional failure in electronic devices. The damage occurs via electron-hole pair production, transport and trapping in the dielectric and interface regions. In discrete devices the bulk of the damage is frequently manifested as a reduction in the gain and/or breakdown voltage of the device. The damage will usually anneal with time following the end of the radiation exposure. Due to this annealing, and to ensure a worst-case test condition MIL-STD-883H TM1019 calls out a dose rate of 50 to $300 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$ as Condition A and further specifies that the time from the end of an incremental radiation exposure and electrical testing shall be 1-hour or less and the total time from the end of one incremental irradiation to the beginning of the next incremental radiation step should be 2-hours or less. The work described in this report was performed to meet MIL-STD-883H TM1019 Condition A.

### 2.0. Radiation Test Apparatus

The total ionizing dose testing described in this final report was performed using the facilities at Aeroflex RAD's Longmire Laboratories in Colorado Springs, CO. The high dose rate total ionizing dose (TID) source is a JLSA 81-24 irradiator modified to provide a panoramic exposure. The Co-60 rods are held in the base of the irradiator heavily shielded by lead. During the radiation exposures the rod is raised by an electronic timer/controller and the exposure is performed in air. The dose rate for this irradiator in this configuration ranges from <1rad(Si)/s to a maximum of approximately $300 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$, determined by the distance from the source. For high-dose rate experiments the bias boards are placed in a radial fashion equidistant from the raised Co-60 rods with the distance adjusted to provide the required dose rate. The irradiator calibration is maintained by Aeroflex RAD Longmire Laboratories using air ionization chamber (AIC) equipment calibrated with traceability to the National Institute of Standards and Technology (NIST). Figure 2.1 shows a photograph of the JLSA 81-24 Co-60 irradiator at Aeroflex RAD's Longmire Laboratory facility.

Aeroflex RAD is currently certified by the Defense Logistics Agency (DLA) for Laboratory Suitability under MIL STD 750 and MIL-STD-883H. Additional details regarding Aeroflex RAD dosimetry for TM1019 Condition A testing are available in Aeroflex RAD's report to DLA entitled: "Dose Rate Mapping of the J.L. Shepherd and Associates Model 81 Irradiator Installed by Radiation Assured Devices".

TID Report<br>15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 2.1. Aeroflex RAD's high dose rate Co-60 irradiator. The dose rate is obtained by positioning the device-under-test at a fixed distance from the gamma cell. The dose rate for this irradiator varies from approximately $300 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$ close to the rods down to $1 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$ at a distance of approximately 2 -feet.

TID Report 15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800

### 3.0. Radiation Test Conditions

The RH1056AMW Precision, High Speed, JFET Input Operational Amplifier described in this final report were irradiated using a split 15 V supply and with all pins tied to ground, that is biased and unbiased. See the TID Bias Table in Appendix B for the full bias circuits. In our opinion, this bias circuit satisfies the requirements of MIL-STD-883H TM1019 Section 3.9.3 Bias and Loading Conditions which states "The bias applied to the test devices shall be selected to produce the greatest radiation induced damage or the worst-case damage for the intended application, if known. While maximum voltage is often worst case some bipolar linear device parameters (e.g. input bias current or maximum output load current) exhibit more degradation with 0 V bias."

The devices were irradiated to a maximum total ionizing dose level of $100 \mathrm{krad}(\mathrm{Si})$ with incremental readings at $10 \mathrm{krad}(\mathrm{Si}), 20 \mathrm{krad}(\mathrm{Si})$, $30 \mathrm{krad}(\mathrm{Si})$ and $50 \mathrm{krad}(\mathrm{Si})$. Electrical testing occurred within one hour following the end of each irradiation segment. For intermediate irradiations, the parts were tested and returned to total dose exposure within two hours from the end of the previous radiation increment.

The TID bias board was positioned in the Co-60 cell to provide the required minimum of $50 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$ and was located inside a lead-aluminum enclosure. The lead-aluminum enclosure is required under MIL-STD-883H TM1019 Section 3.4 that reads as follows: "Lead/Aluminum ( $\mathrm{Pb} / \mathrm{Al}$ ) container. Test specimens shall be enclosed in a $\mathrm{Pb} / \mathrm{Al}$ container to minimize dose enhancement effects caused by lowenergy, scattered radiation. A minimum of 1.5 mm Pb , surrounding an inner shield of at least 0.7 mm Al , is required. This $\mathrm{Pb} / \mathrm{Al}$ container produces an approximate charged particle equilibrium for Si and for TLDs such as CaF 2 . The radiation field intensity shall be measured inside the $\mathrm{Pb} / \mathrm{Al}$ container (1) initially, (2) when the source is changed, or (3) when the orientation or configuration of the source, container, or test-fixture is changed. This measurement shall be performed by placing a dosimeter (e.g., a TLD) in the device-irradiation container at the approximate test-device position. If it can be demonstrated that low energy scattered radiation is small enough that it will not cause dosimetry errors due to dose enhancement, the $\mathrm{Pb} / \mathrm{Al}$ container may be omitted."

The final dose rate within the high dose rate lead-aluminum enclosure was determined using calibration calculations based on air ionization chamber (AIC) dosimetry performed just prior to beginning the total dose irradiations. The final dose rate for this work was $51.8 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$ with a precision of $\pm 5 \%$.

## TID Report 15-0704 07/12/16 R1.1

## Aeroflex RAD

 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800
### 4.0. Tested Parameters

During the total ionizing dose characterization testing the following electrical parameters were measured pre- and post-irradiation:

1. Positive Supply Current (A) @ VS=+/-15V, VCM=0V
2. Negative Supply Current (A) @ VS=+/-15V, VCM=0V
3. Input Offset Voltage (V) @ VS=+/-15V, VCM=0V
4. Input Offset Current (A) @ VS=+/-15V, VCM=0V
5. Positive Input Bias Current (A) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$
6. Negative Input Bias Current (A) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$
7. Large Signal Voltage Gain1 (V/mV) @ VS=+/-15V, VO=+/-10V, RL=2k $\Omega$
8. Large Signal Voltage Gain2 (V/mV) @ VS=+/-15V, VO=+/-10V, RL=1k $\Omega$
9. Common Mode Rejection Ratio (dB) @ VS=+/-15V, VCM=+/-11V
10. Power Supply Rejection Ratio (dB) @ VS=+/-10 To +/-18V
11. Positive Slew Rate (V/ $\mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$
12. Negative Slew Rate ( $\mathrm{V} / \mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$
13. Positive Output Voltage Swing (V) @ VS=+/-15V, RL=2k $\Omega$
14. Negative Output Voltage Swing (V) @ VS=+/-15V, RL=2k $\Omega$

Appendix C details the measured parameters, test conditions, pre-irradiation specification and measurement resolution for each of the measurements.

The parametric data was obtained as "read and record" and all the raw data plus an attributes summary are contained in this report as well as in a separate Excel file. The attributes data contains the average, standard deviation and the average with the KTL values applied. The KTL value used in this work is 2.742 per MIL-HDBK-814 using one sided tolerance limits of $90 / 90$ and a 5 -piece sample size. The 90/90 KTL values were selected to match the statistical levels specified in the MIL-PRF-38535 sampling plan for the qualification of a radiation hardness assured (RHA) component. Note that the following criteria must be met for a device to pass the total ionizing dose test: following the radiation exposure each of the 5 pieces irradiated under electrical bias shall pass the specification value. The units irradiated without electrical bias and the KTL statistics are included in this report for reference only. If any of the 5 pieces irradiated under electrical bias exceed the device post radiation data sheet specification limits, then the lot could be logged as a failure.

Further, MIL-STD-883H, TM 1019 Section 3.13.1.1 Characterization test to determine if a part exhibits ELDRS' states the following: Select a minimum random sample of 21 devices from a population representative of recent production runs. Smaller sample sizes may be used if agreed upon between the parties to the test. All of the selected devices shall have undergone appropriate elevated temperature reliability screens, e.g. burn-in and high temperature storage life. Divide the samples into four groups of 5 each and use the remaining part for a control. Perform pre-irradiation electrical characterization on all parts assuring that they meet the Group A electrical tests. Irradiate 5 samples under a 0 volt bias and

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800
another 5 under the irradiation bias given in the acquisition specification at $50-300 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$ and room temperature. Irradiate 5 samples under a 0 volt bias and another 5 under irradiation bias given in the acquisition specification at $<10 \mathrm{mrad}(\mathrm{Si}) / \mathrm{s}$ and room temperature. Irradiate all samples to the same dose levels, including 0.5 and 1.0 times the anticipated specification dose, and repeat the electrical characterization on each part at each dose level. Post irradiation electrical measurements shall be performed per paragraph 3.10 where the low dose rate test is considered Condition D. Calculate the radiation induced change in each electrical parameter ( $\Delta$ para) for each sample at each radiation level. Calculate the ratio of the median $\Delta$ para at low dose rate to the median $\Delta$ para at high dose rate for each irradiation bias group at each total dose level. If this ratio exceeds 1.5 for any of the most sensitive parameters then the part is considered to be ELDRS susceptible. This test does not apply to parameters which exhibit changes that are within experimental error or whose values are below the pre-irradiation electrical specification limits at low dose rate at the specification dose.

Therefore, the data in this report can be analyzed along with the low dose rate report titled "Enhanced Low Dose Rate Sensitivity (ELDRS) Radiation Testing of the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier for Linear Technology" to demonstrate that these parts do not exhibit ELDRS as defined in the current test method.

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800

### 5.0. Total lonizing Dose Test Results

Based on this criterion the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier (from the lot traceability information provided on the first page of this test report) PASSED the total ionizing dose test to the maximum tested dose level of $100 \mathrm{krad}(\mathrm{Si})$ with all parameters remaining within their datasheet specifications.

Figures 5.1 through 5.14 show plots of all the measured parameters versus total ionizing dose while Tables 5.1-5.14 show the corresponding raw data for each of these parameters. In the data plots the solid diamonds are the average of the measured data points for the sample irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the units irradiated with all pins tied to ground. The black lines (solid or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the sample irradiated in the biased condition while the shaded lines (solid or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the sample irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

The control units, as expected, show no significant changes to any of the parameters. Therefore we can conclude that the electrical testing remained in control throughout the duration of the tests and the observed degradation was due to the radiation exposure. Appendix D lists the figures used in this section to facilitate the location of a particular parameter.

TID Report
15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.1. Plot of Positive Supply Current (A) @ VS=+/-15V, VCM=0V versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd.
Colorado Springs, CO 80919
(719) 531-0800

Table 5.1. Raw data for Positive Supply Current (A) @ VS=+/-15V, VCM=0V versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Positive Supply Current (A) @ VS=+/-15V, VCM=0V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | 4.82E-03 | $4.76 \mathrm{E}-03$ | 4.72E-03 | $4.70 \mathrm{E}-03$ | 4.64E-03 | $4.54 \mathrm{E}-03$ |
| 1318 | 4.83E-03 | $4.77 \mathrm{E}-03$ | 4.73E-03 | $4.70 \mathrm{E}-03$ | $4.65 \mathrm{E}-03$ | $4.54 \mathrm{E}-03$ |
| 1321 | $4.70 \mathrm{E}-03$ | 4.63E-03 | $4.60 \mathrm{E}-03$ | 4.57E-03 | 4.52E-03 | $4.41 \mathrm{E}-03$ |
| 1322 | $4.60 \mathrm{E}-03$ | 4.53E-03 | $4.50 \mathrm{E}-03$ | 4.47E-03 | $4.42 \mathrm{E}-03$ | $4.32 \mathrm{E}-03$ |
| 1323 | 4.62E-03 | $4.56 \mathrm{E}-03$ | $4.51 \mathrm{E}-03$ | $4.49 \mathrm{E}-03$ | $4.43 \mathrm{E}-03$ | $4.33 \mathrm{E}-03$ |
| 1324 | $4.58 \mathrm{E}-03$ | 4.55E-03 | 4.54E-03 | 4.52E-03 | $4.48 \mathrm{E}-03$ | $4.39 \mathrm{E}-03$ |
| 1325 | $4.68 \mathrm{E}-03$ | $4.65 \mathrm{E}-03$ | 4.62E-03 | $4.60 \mathrm{E}-03$ | 4.57E-03 | $4.48 \mathrm{E}-03$ |
| 1326 | 4.89E-03 | 4.87E-03 | 4.85E-03 | 4.83E-03 | 4.79E-03 | $4.69 \mathrm{E}-03$ |
| 1327 | $4.86 \mathrm{E}-03$ | 4.83E-03 | $4.81 \mathrm{E}-03$ | 4.79E-03 | $4.76 \mathrm{E}-03$ | $4.68 \mathrm{E}-03$ |
| 1328 | 4.86E-03 | 4.83E-03 | 4.79E-03 | 4.79E-03 | $4.76 \mathrm{E}-03$ | $4.68 \mathrm{E}-03$ |
| 1329 | 4.91E-03 | 4.92E-03 | $4.91 \mathrm{E}-03$ | $4.91 \mathrm{E}-03$ | $4.91 \mathrm{E}-03$ | $4.91 \mathrm{E}-03$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | 4.71E-03 | 4.65E-03 | 4.61E-03 | 4.59E-03 | 4.53E-03 | 4.43E-03 |
| Std Dev Biased | $1.09 \mathrm{E}-04$ | $1.11 \mathrm{E}-04$ | 1.12E-04 | 1.12E-04 | 1.12E-04 | 1.09E-04 |
| Ps90\%/90\% (+KTL) Biased | $5.01 \mathrm{E}-03$ | $4.95 \mathrm{E}-03$ | 4.92E-03 | $4.89 \mathrm{E}-03$ | $4.84 \mathrm{E}-03$ | $4.73 \mathrm{E}-03$ |
| Ps90\%/90\% (-KTL) Biased | 4.41E-03 | $4.34 \mathrm{E}-03$ | 4.31E-03 | $4.28 \mathrm{E}-03$ | 4.22E-03 | $4.13 \mathrm{E}-03$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | 4.77E-03 | 4.75E-03 | 4.72E-03 | 4.70E-03 | 4.67E-03 | $4.58 \mathrm{E}-03$ |
| Std Dev Un-Biased | $1.38 \mathrm{E}-04$ | $1.38 \mathrm{E}-04$ | $1.35 \mathrm{E}-04$ | $1.37 \mathrm{E}-04$ | $1.38 \mathrm{E}-04$ | $1.40 \mathrm{E}-04$ |
| Ps90\%/90\% (+KTL) Un-Biased | 5.15E-03 | $5.12 \mathrm{E}-03$ | 5.09E-03 | $5.08 \mathrm{E}-03$ | 5.05E-03 | 4.97E-03 |
| Ps90\%/90\% (-KTL) Un-Biased | $4.40 \mathrm{E}-03$ | 4.37E-03 | 4.35E-03 | 4.33E-03 | $4.29 \mathrm{E}-03$ | $4.20 \mathrm{E}-03$ |
| Specification MAX | 6.50E-03 | $7.00 \mathrm{E}-03$ | 7.00E-03 | $7.00 \mathrm{E}-03$ | $7.00 \mathrm{E}-03$ | $7.00 \mathrm{E}-03$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

TID Report 15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.2. Plot of Negative Supply Current (A) @ VS=+/-15V, VCM=0V versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd.
Colorado Springs, CO 80919
(719) 531-0800

Table 5.2. Raw data for Negative Supply Current (A) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Negative Supply Current (A) @ VS=+/-15V, VCM=0V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | -4.82E-03 | -4.75E-03 | -4.73E-03 | -4.70E-03 | -4.65E-03 | -4.54E-03 |
| 1318 | -4.83E-03 | -4.76E-03 | -4.74E-03 | -4.70E-03 | -4.65E-03 | -4.55E-03 |
| 1321 | -4.70E-03 | -4.64E-03 | -4.60E-03 | -4.58E-03 | -4.52E-03 | -4.42E-03 |
| 1322 | -4.60E-03 | -4.53E-03 | -4.50E-03 | -4.47E-03 | -4.42E-03 | -4.32E-03 |
| 1323 | -4.62E-03 | -4.56E-03 | -4.51E-03 | -4.49E-03 | -4.43E-03 | -4.34E-03 |
| 1324 | -4.58E-03 | -4.55E-03 | -4.54E-03 | -4.52E-03 | -4.48E-03 | -4.39E-03 |
| 1325 | -4.68E-03 | -4.66E-03 | -4.63E-03 | -4.61E-03 | -4.57E-03 | -4.47E-03 |
| 1326 | -4.90E-03 | -4.87E-03 | -4.85E-03 | -4.83E-03 | -4.79E-03 | -4.70E-03 |
| 1327 | -4.85E-03 | -4.83E-03 | -4.82E-03 | -4.80E-03 | -4.75E-03 | -4.67E-03 |
| 1328 | -4.85E-03 | -4.83E-03 | $-4.79 \mathrm{E}-03$ | -4.80E-03 | -4.76E-03 | -4.68E-03 |
| 1329 | -4.91E-03 | -4.92E-03 | -4.92E-03 | -4.91E-03 | -4.92E-03 | -4.91E-03 |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | -4.71E-03 | -4.65E-03 | -4.62E-03 | -4.59E-03 | -4.53E-03 | -4.43E-03 |
| Std Dev Biased | $1.08 \mathrm{E}-04$ | 1.08E-04 | 1.13E-04 | 1.12E-04 | 1.11E-04 | 1.11E-04 |
| Ps90\%/90\% (+KTL) Biased | -4.42E-03 | -4.35E-03 | -4.31E-03 | -4.28E-03 | -4.23E-03 | -4.13E-03 |
| Ps90\%/90\% (-KTL) Biased | -5.01E-03 | -4.95E-03 | -4.93E-03 | -4.89E-03 | -4.84E-03 | -4.74E-03 |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | -4.77E-03 | -4.75E-03 | -4.72E-03 | -4.71E-03 | -4.67E-03 | -4.58E-03 |
| Std Dev Un-Biased | 1.36E-04 | 1.38E-04 | 1.32E-04 | 1.37E-04 | 1.37E-04 | 1.42E-04 |
| Ps90\%/90\% (+KTL) Un-Biased | -4.40E-03 | -4.37E-03 | -4.36E-03 | -4.33E-03 | -4.30E-03 | -4.19E-03 |
| Ps90\%/90\% (-KTL) Un-Biased | -5.15E-03 | -5.13E-03 | -5.09E-03 | -5.09E-03 | -5.05E-03 | -4.97E-03 |
| Specification MIN | -6.50E-03 | -7.00E-03 | -7.00E-03 | -7.00E-03 | -7.00E-03 | -7.00E-03 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

TID Report
15-0704 07/12/16 R1.1
Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.3. Plot of Input Offset Voltage (V) @ VS=+/-15V, VCM=0V versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.3. Raw data for Input Offset Voltage (V) @ VS=+/-15V, VCM=0V versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Input Offset Voltage (V) @ VS=+/-15V, VCM=0V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | -2.12E-04 | -2.38E-04 | -2.71E-04 | -2.86E-04 | -3.11E-04 | -3.48E-04 |
| 1318 | 7.91E-05 | $7.40 \mathrm{E}-05$ | 5.11E-05 | $2.71 \mathrm{E}-05$ | 9.66E-06 | -1.79E-05 |
| 1321 | -5.32E-05 | -5.41E-05 | -8.27E-05 | -1.00E-04 | -1.20E-04 | -1.48E-04 |
| 1322 | -1.23E-04 | -1.40E-04 | -1.63E-04 | -1.78E-04 | -1.96E-04 | -2.30E-04 |
| 1323 | -1.43E-04 | -1.54E-04 | -1.69E-04 | -1.77E-04 | -1.86E-04 | -2.12E-04 |
| 1324 | -2.27E-06 | -1.86E-05 | -3.43E-05 | -6.32E-05 | -9.19E-05 | -1.52E-04 |
| 1325 | -7.09E-05 | -7.71E-05 | -1.00E-04 | -1.20E-04 | -1.54E-04 | -2.00E-04 |
| 1326 | 2.05E-04 | 1.92E-04 | 1.59E-04 | 1.40E-04 | 9.60E-05 | $5.48 \mathrm{E}-05$ |
| 1327 | $1.94 \mathrm{E}-04$ | $1.64 \mathrm{E}-04$ | $1.46 \mathrm{E}-04$ | $1.09 \mathrm{E}-04$ | 8.37E-05 | $2.36 \mathrm{E}-05$ |
| 1328 | -2.62E-04 | -2.79E-04 | -3.19E-04 | -3.33E-04 | -3.75E-04 | -4.38E-04 |
| 1329 | 2.51E-04 | 2.57E-04 | 2.61E-04 | 2.58E-04 | $2.54 \mathrm{E}-04$ | $2.58 \mathrm{E}-04$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | -9.05E-05 | -1.02E-04 | -1.27E-04 | -1.43E-04 | -1.61E-04 | -1.91E-04 |
| Std Dev Biased | $1.10 \mathrm{E}-04$ | 1.18E-04 | 1.20E-04 | 1.16E-04 | 1.18E-04 | $1.21 \mathrm{E}-04$ |
| Ps90\%/90\% (+KTL) Biased | 2.12E-04 | 2.22E-04 | 2.02E-04 | 1.75E-04 | 1.61E-04 | $1.40 \mathrm{E}-04$ |
| Ps90\%/90\% (-KTL) Biased | -3.93E-04 | -4.26E-04 | -4.56E-04 | -4.60E-04 | -4.83E-04 | -5.22E-04 |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $1.28 \mathrm{E}-05$ | -3.86E-06 | -2.96E-05 | -5.34E-05 | -8.82E-05 | -1.42E-04 |
| Std Dev Un-Biased | 1.95E-04 | 1.92E-04 | $1.97 \mathrm{E}-04$ | 1.92E-04 | 1.94E-04 | $1.98 \mathrm{E}-04$ |
| Ps90\%/90\% (+KTL) Un-Biased | 5.48E-04 | 5.23E-04 | $5.10 \mathrm{E}-04$ | 4.72E-04 | 4.42E-04 | 4.01E-04 |
| Ps90\%/90\% (-KTL) Un-Biased | -5.22E-04 | -5.30E-04 | -5.69E-04 | -5.79E-04 | -6.19E-04 | -6.86E-04 |
| Specification MIN | -3.00E-04 | -3.00E-04 | -3.00E-04 | -3.00E-04 | -3.70E-04 | -5.70E-04 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |
| Specification MAX | 3.00E-04 | 3.00E-04 | 3.00E-04 | 3.00E-04 | 3.70E-04 | 5.70E-04 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

TID Report
15-0704 07/12/16 R1.1
Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.4. Plot of Input Offset Current (A) @ VS=+/-15V, VCM=0V versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.4. Raw data for Input Offset Current (A) @ VS=+/-15V, VCM=0V versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Input Offset Current (A) <br> @ VS=+/-15V, VCM=0V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | -8.10E-13 | -2.04E-12 | -6.17E-12 | -9.20E-12 | -1.95E-11 | -4.24E-11 |
| 1318 | -7.80E-13 | -2.90E-12 | -4.32E-12 | -9.41E-12 | -1.80E-11 | -4.03E-11 |
| 1321 | -1.31E-12 | -1.59E-12 | -5.07E-12 | $-1.07 \mathrm{E}-11$ | -1.73E-11 | -4.14E-11 |
| 1322 | -1.22E-12 | -2.88E-12 | -5.59E-12 | -9.26E-12 | -1.99E-11 | -3.90E-11 |
| 1323 | $1.09 \mathrm{E}-12$ | -6.20E-13 | -2.93E-12 | -9.41E-12 | -1.79E-11 | -3.69E-11 |
| 1324 | -5.40E-13 | -2.15E-12 | -1.47E-12 | -3.17E-12 | -5.54E-12 | -7.97E-12 |
| 1325 | -6.20E-13 | -1.20E-12 | -1.19E-12 | -1.34E-12 | -3.81E-12 | -5.40E-12 |
| 1326 | -1.60E-13 | -8.40E-13 | -8.70E-13 | -1.98E-12 | -2.58E-12 | -5.94E-12 |
| 1327 | $4.60 \mathrm{E}-13$ | 1.60E-13 | -8.40E-13 | $-1.00 \mathrm{E}-12$ | -2.26E-12 | -4.68E-12 |
| 1328 | -7.60E-13 | -1.25E-12 | -6.80E-13 | $-1.68 \mathrm{E}-12$ | -2.74E-12 | -6.24E-12 |
| 1329 | $7.20 \mathrm{E}-13$ | 7.10E-13 | $5.90 \mathrm{E}-13$ | 6.10E-13 | 7.10E-13 | 7.00E-13 |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | -6.06E-13 | -2.01E-12 | -4.82E-12 | -9.60E-12 | -1.85E-11 | -4.00E-11 |
| Std Dev Biased | $9.77 \mathrm{E}-13$ | 9.56E-13 | $1.25 \mathrm{E}-12$ | $6.37 \mathrm{E}-13$ | $1.09 \mathrm{E}-12$ | $2.16 \mathrm{E}-12$ |
| Ps90\%/90\% (+KTL) Biased | $2.07 \mathrm{E}-12$ | 6.16E-13 | -1.37E-12 | -7.85E-12 | -1.55E-11 | -3.41E-11 |
| Ps90\%/90\% (-KTL) Biased | -3.29E-12 | -4.63E-12 | -8.26E-12 | -1.13E-11 | -2.15E-11 | -4.59E-11 |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | -3.24E-13 | -1.06E-12 | -1.01E-12 | -1.83E-12 | -3.39E-12 | -6.05E-12 |
| Std Dev Un-Biased | $4.91 \mathrm{E}-13$ | 8.34E-13 | 3.17E-13 | $8.32 \mathrm{E}-13$ | $1.34 \mathrm{E}-12$ | 1.23E-12 |
| Ps90\%/90\% (+KTL) Un-Biased | $1.02 \mathrm{E}-12$ | 1.23E-12 | -1.41E-13 | $4.48 \mathrm{E}-13$ | $2.81 \mathrm{E}-13$ | -2.68E-12 |
| Ps90\%/90\% (-KTL) Un-Biased | -1.67E-12 | -3.34E-12 | -1.88E-12 | -4.12E-12 | -7.05E-12 | -9.41E-12 |
| Specification MIN | -1.00E-11 | -1.00E-11 | -5.00E-11 | -5.00E-11 | -1.50E-10 | -2.50E-10 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |
| Specification MAX | $1.00 \mathrm{E}-11$ | 1.00E-11 | 5.00E-11 | 5.00E-11 | 1.50E-10 | 2.50E-10 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

TID Report
15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.5. Plot of Positive Input Bias Current (A) @ VS $=+/-15 \mathrm{~V}$, $\mathrm{VCM}=0 \mathrm{~V}$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.5. Raw data for Positive Input Bias Current (A) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Positive Input Bias Current (A) <br> @ VS=+/-15V, VCM=0V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $9.05 \mathrm{E}-12$ | $1.98 \mathrm{E}-11$ | $3.78 \mathrm{E}-11$ | $6.47 \mathrm{E}-11$ | $1.11 \mathrm{E}-10$ | $2.68 \mathrm{E}-10$ |
| 1318 | $8.59 \mathrm{E}-12$ | $2.12 \mathrm{E}-11$ | $3.71 \mathrm{E}-11$ | $6.10 \mathrm{E}-11$ | $1.05 \mathrm{E}-10$ | $2.48 \mathrm{E}-10$ |
| 1321 | $1.21 \mathrm{E}-11$ | $2.59 \mathrm{E}-11$ | $3.86 \mathrm{E}-11$ | $6.51 \mathrm{E}-11$ | $1.05 \mathrm{E}-10$ | $2.34 \mathrm{E}-10$ |
| 1322 | 9.35E-12 | 1.99E-11 | $3.50 \mathrm{E}-11$ | 5.60E-11 | $1.02 \mathrm{E}-10$ | $2.22 \mathrm{E}-10$ |
| 1323 | $1.24 \mathrm{E}-11$ | 2.95E-11 | 5.07E-11 | 6.92E-11 | $1.04 \mathrm{E}-10$ | $2.20 \mathrm{E}-10$ |
| 1324 | 9.20E-12 | $1.41 \mathrm{E}-11$ | $1.76 \mathrm{E}-11$ | 2.56E-11 | $3.36 \mathrm{E}-11$ | $5.98 \mathrm{E}-11$ |
| 1325 | $8.89 \mathrm{E}-12$ | $1.30 \mathrm{E}-11$ | $2.03 \mathrm{E}-11$ | $2.71 \mathrm{E}-11$ | 3.43E-11 | $6.08 \mathrm{E}-11$ |
| 1326 | 9.70E-12 | $1.63 \mathrm{E}-11$ | $2.21 \mathrm{E}-11$ | $3.01 \mathrm{E}-11$ | $3.81 \mathrm{E}-11$ | $6.45 \mathrm{E}-11$ |
| 1327 | $8.74 \mathrm{E}-12$ | $1.27 \mathrm{E}-11$ | 2.10E-11 | $2.81 \mathrm{E}-11$ | $3.89 \mathrm{E}-11$ | $6.17 \mathrm{E}-11$ |
| 1328 | $8.28 \mathrm{E}-12$ | $1.41 \mathrm{E}-11$ | $2.13 \mathrm{E}-11$ | $2.71 \mathrm{E}-11$ | $3.66 \mathrm{E}-11$ | $6.26 \mathrm{E}-11$ |
| 1329 | $7.64 \mathrm{E}-12$ | 8.09E-12 | $8.74 \mathrm{E}-12$ | $9.11 \mathrm{E}-12$ | $6.35 \mathrm{E}-12$ | 6.35E-12 |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $1.03 \mathrm{E}-11$ | $2.33 \mathrm{E}-11$ | 3.98E-11 | $6.32 \mathrm{E}-11$ | $1.06 \mathrm{E}-10$ | $2.38 \mathrm{E}-10$ |
| Std Dev Biased | $1.81 \mathrm{E}-12$ | $4.27 \mathrm{E}-12$ | $6.22 \mathrm{E}-12$ | $4.97 \mathrm{E}-12$ | $3.35 \mathrm{E}-12$ | $2.00 \mathrm{E}-11$ |
| Ps90\%/90\% (+KTL) Biased | $1.53 \mathrm{E}-11$ | $3.50 \mathrm{E}-11$ | 5.69E-11 | $7.68 \mathrm{E}-11$ | $1.15 \mathrm{E}-10$ | $2.93 \mathrm{E}-10$ |
| Ps90\%/90\% (-KTL) Biased | 5.33E-12 | $1.16 \mathrm{E}-11$ | $2.28 \mathrm{E}-11$ | 4.96E-11 | $9.64 \mathrm{E}-11$ | $1.84 \mathrm{E}-10$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $8.96 \mathrm{E}-12$ | $1.41 \mathrm{E}-11$ | $2.05 \mathrm{E}-11$ | $2.76 \mathrm{E}-11$ | 3.63E-11 | 6.19E-11 |
| Std Dev Un-Biased | $5.29 \mathrm{E}-13$ | $1.38 \mathrm{E}-12$ | $1.70 \mathrm{E}-12$ | $1.69 \mathrm{E}-12$ | $2.30 \mathrm{E}-12$ | $1.80 \mathrm{E}-12$ |
| Ps90\%/90\% (+KTL) Un-Biased | $1.04 \mathrm{E}-11$ | $1.78 \mathrm{E}-11$ | $2.51 \mathrm{E}-11$ | 3.22E-11 | $4.26 \mathrm{E}-11$ | $6.68 \mathrm{E}-11$ |
| Ps90\%/90\% (-KTL) Un-Biased | $7.51 \mathrm{E}-12$ | $1.03 \mathrm{E}-11$ | $1.58 \mathrm{E}-11$ | $2.30 \mathrm{E}-11$ | $3.00 \mathrm{E}-11$ | $5.69 \mathrm{E}-11$ |
| Specification MIN | -5.00E-11 | 5.00E-11 | -2.50E-10 | -2.50E-10 | 5.00E-10 | -1.00E-09 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |
| Specification MAX | $5.00 \mathrm{E}-11$ | $5.00 \mathrm{E}-11$ | 2.50E-10 | $2.50 \mathrm{E}-10$ | 5.00E-10 | 1.00E-09 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

TID Report
15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.6. Plot of Negative Input Bias Current (A) @ VS=+/-15V, VCM=0V versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd.
Colorado Springs, CO 80919
(719) 531-0800

Table 5.6. Raw data for Negative Input Bias Current (A) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Negative Input Bias Current (A) <br> @ VS=+/-15V, VCM=0V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $1.06 \mathrm{E}-11$ | $2.41 \mathrm{E}-11$ | $4.32 \mathrm{E}-11$ | 7.43E-11 | $1.31 \mathrm{E}-10$ | $3.12 \mathrm{E}-10$ |
| 1318 | $9.56 \mathrm{E}-12$ | $2.27 \mathrm{E}-11$ | $4.30 \mathrm{E}-11$ | $6.92 \mathrm{E}-11$ | $1.24 \mathrm{E}-10$ | 2.89E-10 |
| 1321 | 1.22E-11 | $2.76 \mathrm{E}-11$ | $4.40 \mathrm{E}-11$ | $7.22 \mathrm{E}-11$ | $1.21 \mathrm{E}-10$ | $2.77 \mathrm{E}-10$ |
| 1322 | $9.26 \mathrm{E}-12$ | 2.15E-11 | 4.15E-11 | $6.51 \mathrm{E}-11$ | $1.16 \mathrm{E}-10$ | $2.65 \mathrm{E}-10$ |
| 1323 | $1.18 \mathrm{E}-11$ | $2.90 \mathrm{E}-11$ | 5.17E-11 | $7.73 \mathrm{E}-11$ | $1.25 \mathrm{E}-10$ | $2.56 \mathrm{E}-10$ |
| 1324 | $1.04 \mathrm{E}-11$ | $1.37 \mathrm{E}-11$ | 2.07E-11 | $2.65 \mathrm{E}-11$ | 3.63E-11 | $6.64 \mathrm{E}-11$ |
| 1325 | $8.38 \mathrm{E}-12$ | 1.37E-11 | $2.03 \mathrm{E}-11$ | $2.78 \mathrm{E}-11$ | 3.85E-11 | $6.83 \mathrm{E}-11$ |
| 1326 | $8.38 \mathrm{E}-12$ | 1.67E-11 | $2.31 \mathrm{E}-11$ | $3.21 \mathrm{E}-11$ | $4.35 \mathrm{E}-11$ | 7.10E-11 |
| 1327 | 8.67E-12 | $1.30 \mathrm{E}-11$ | 2.13E-11 | $2.88 \mathrm{E}-11$ | $4.07 \mathrm{E}-11$ | $6.54 \mathrm{E}-11$ |
| 1328 | 7.65E-12 | 1.49E-11 | 2.35E-11 | 2.90E-11 | $4.02 \mathrm{E}-11$ | $6.54 \mathrm{E}-11$ |
| 1329 | $7.65 \mathrm{E}-12$ | $8.09 \mathrm{E}-12$ | 8.17E-12 | 9.26E-12 | $6.89 \mathrm{E}-12$ | $7.56 \mathrm{E}-12$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $1.07 \mathrm{E}-11$ | 2.50E-11 | $4.47 \mathrm{E}-11$ | 7.16E-11 | 1.23E-10 | $2.80 \mathrm{E}-10$ |
| Std Dev Biased | $1.30 \mathrm{E}-12$ | $3.21 \mathrm{E}-12$ | $4.03 \mathrm{E}-12$ | $4.70 \mathrm{E}-12$ | $5.41 \mathrm{E}-12$ | $2.18 \mathrm{E}-11$ |
| Ps90\%/90\% (+KTL) Biased | $1.42 \mathrm{E}-11$ | 3.38E-11 | $5.57 \mathrm{E}-11$ | $8.45 \mathrm{E}-11$ | 1.38E-10 | $3.39 \mathrm{E}-10$ |
| Ps90\%/90\% (-KTL) Biased | $7.11 \mathrm{E}-12$ | 1.62E-11 | 3.36E-11 | $5.87 \mathrm{E}-11$ | 1.08E-10 | $2.20 \mathrm{E}-10$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | 8.70E-12 | $1.44 \mathrm{E}-11$ | $2.18 \mathrm{E}-11$ | $2.88 \mathrm{E}-11$ | 3.99E-11 | $6.73 \mathrm{E}-11$ |
| Std Dev Un-Biased | $1.04 \mathrm{E}-12$ | 1.47E-12 | $1.44 \mathrm{E}-12$ | $2.07 \mathrm{E}-12$ | $2.68 \mathrm{E}-12$ | $2.39 \mathrm{E}-12$ |
| Ps90\%/90\% (+KTL) Un-Biased | $1.16 \mathrm{E}-11$ | $1.84 \mathrm{E}-11$ | $2.57 \mathrm{E}-11$ | $3.45 \mathrm{E}-11$ | $4.72 \mathrm{E}-11$ | 7.38E-11 |
| Ps90\%/90\% (-KTL) Un-Biased | $5.85 \mathrm{E}-12$ | $1.04 \mathrm{E}-11$ | $1.78 \mathrm{E}-11$ | $2.31 \mathrm{E}-11$ | $3.25 \mathrm{E}-11$ | $6.08 \mathrm{E}-11$ |
| Specification MIN | -5.00E-11 | -5.00E-11 | -2.50E-10 | -2.50E-10 | -5.00E-10 | -1.00E-09 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |
| Specification MAX | $5.00 \mathrm{E}-11$ | 5.00E-11 | $2.50 \mathrm{E}-10$ | $2.50 \mathrm{E}-10$ | 5.00E-10 | 1.00E-09 |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company


Figure 5.7. Plot of Large Signal Voltage Gain1 (V/mV) @ VS=+/-15V, VO=+/-10V, RL=2k $\Omega$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aleroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.7. Raw data for Large Signal Voltage Gain1 (V/mV) @ VS $=+/-15 \mathrm{~V}, \mathrm{VO}=+/-10 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Large Signal Voltage Gain1 (V/mV) <br> @ VS=+/-15V, VO=+/-10V, RL=2k $\Omega$ | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $2.82 \mathrm{E}+02$ | $2.77 \mathrm{E}+02$ | $2.81 \mathrm{E}+02$ | $2.81 \mathrm{E}+02$ | $2.83 \mathrm{E}+02$ | $2.79 \mathrm{E}+02$ |
| 1318 | $2.98 \mathrm{E}+02$ | $2.92 \mathrm{E}+02$ | $2.99 \mathrm{E}+02$ | $2.95 \mathrm{E}+02$ | $2.92 \mathrm{E}+02$ | $2.95 \mathrm{E}+02$ |
| 1321 | $2.74 \mathrm{E}+02$ | $2.70 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ | $2.73 \mathrm{E}+02$ | $2.77 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ |
| 1322 | $2.91 \mathrm{E}+02$ | $2.81 \mathrm{E}+02$ | $2.88 \mathrm{E}+02$ | $2.86 \mathrm{E}+02$ | $2.83 \mathrm{E}+02$ | $2.89 \mathrm{E}+02$ |
| 1323 | $2.66 \mathrm{E}+02$ | $2.63 \mathrm{E}+02$ | $2.60 \mathrm{E}+02$ | $2.64 \mathrm{E}+02$ | $2.62 \mathrm{E}+02$ | $2.56 \mathrm{E}+02$ |
| 1324 | $2.90 \mathrm{E}+02$ | $2.87 \mathrm{E}+02$ | $2.82 \mathrm{E}+02$ | $2.84 \mathrm{E}+02$ | $2.89 \mathrm{E}+02$ | $2.79 \mathrm{E}+02$ |
| 1325 | 2.97E+02 | 2.92E+02 | $2.91 \mathrm{E}+02$ | $2.90 \mathrm{E}+02$ | $2.94 \mathrm{E}+02$ | $2.85 \mathrm{E}+02$ |
| 1326 | $2.58 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.54 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.56 \mathrm{E}+02$ | $2.59 \mathrm{E}+02$ |
| 1327 | $2.60 \mathrm{E}+02$ | $2.60 \mathrm{E}+02$ | $2.60 \mathrm{E}+02$ | $2.63 \mathrm{E}+02$ | $2.56 \mathrm{E}+02$ | $2.62 \mathrm{E}+02$ |
| 1328 | $2.78 \mathrm{E}+02$ | $2.78 \mathrm{E}+02$ | $2.69 \mathrm{E}+02$ | $2.73 \mathrm{E}+02$ | $2.77 \mathrm{E}+02$ | $2.77 \mathrm{E}+02$ |
| 1329 | $2.54 \mathrm{E}+02$ | $2.59 \mathrm{E}+02$ | $2.59 \mathrm{E}+02$ | $2.61 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.54 \mathrm{E}+02$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $2.82 \mathrm{E}+02$ | $2.76 \mathrm{E}+02$ | $2.80 \mathrm{E}+02$ | $2.79 \mathrm{E}+02$ | $2.79 \mathrm{E}+02$ | $2.79 \mathrm{E}+02$ |
| Std Dev Biased | $1.29 \mathrm{E}+01$ | $1.10 \mathrm{E}+01$ | $1.46 \mathrm{E}+01$ | $1.20 \mathrm{E}+01$ | 1.12E+01 | $1.51 \mathrm{E}+01$ |
| Ps90\%/90\% (+KTL) Biased | $3.17 \mathrm{E}+02$ | 3.07E+02 | $3.20 \mathrm{E}+02$ | $3.12 \mathrm{E}+02$ | $3.10 \mathrm{E}+02$ | $3.20 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Biased | $2.47 \mathrm{E}+02$ | $2.46 \mathrm{E}+02$ | $2.40 \mathrm{E}+02$ | $2.47 \mathrm{E}+02$ | $2.49 \mathrm{E}+02$ | $2.37 \mathrm{E}+02$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $2.77 \mathrm{E}+02$ | $2.75 \mathrm{E}+02$ | $2.71 \mathrm{E}+02$ | $2.73 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ | $2.72 \mathrm{E}+02$ |
| Std Dev Un-Biased | $1.73 \mathrm{E}+01$ | $1.59 \mathrm{E}+01$ | $1.52 \mathrm{E}+01$ | $1.42 \mathrm{E}+01$ | $1.78 \mathrm{E}+01$ | $1.15 \mathrm{E}+01$ |
| Ps90\%/90\% (+KTL) Un-Biased | $3.24 \mathrm{E}+02$ | 3.18E+02 | $3.13 \mathrm{E}+02$ | $3.12 \mathrm{E}+02$ | $3.23 \mathrm{E}+02$ | $3.04 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Un-Biased | $2.29 \mathrm{E}+02$ | $2.31 \mathrm{E}+02$ | $2.29 \mathrm{E}+02$ | $2.34 \mathrm{E}+02$ | $2.25 \mathrm{E}+02$ | $2.41 \mathrm{E}+02$ |
| Specification MIN | $1.50 \mathrm{E}+02$ | $1.50 \mathrm{E}+02$ | $1.50 \mathrm{E}+02$ | $1.50 \mathrm{E}+02$ | $1.50 \mathrm{E}+02$ | $1.00 \mathrm{E}+02$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |



Figure 5.8. Plot of Large Signal Voltage Gain2 (V/mV) @ VS=+/-15V, VO=+/-10V, RL=1k $\Omega$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.8. Raw data for Large Signal Voltage Gain2 (V/mV) @ VS $=+/-15 \mathrm{~V}, \mathrm{VO}=+/-10 \mathrm{~V}, \mathrm{RL}=1 \mathrm{k} \Omega$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Large Signal Voltage Gain2 (V/mV) @ VS=+/-15V, VO=+/-10V, RL=1k | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | 2.67E+02 | $2.61 \mathrm{E}+02$ | $2.63 \mathrm{E}+02$ | $2.66 \mathrm{E}+02$ | $2.66 \mathrm{E}+02$ | $2.64 \mathrm{E}+02$ |
| 1318 | $2.79 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ | $2.79 \mathrm{E}+02$ | 2.77E+02 | $2.71 \mathrm{E}+02$ |
| 1321 | $2.54 \mathrm{E}+02$ | $2.50 \mathrm{E}+02$ | $2.58 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.54 \mathrm{E}+02$ |
| 1322 | $2.73 \mathrm{E}+02$ | $2.66 \mathrm{E}+02$ | $2.71 \mathrm{E}+02$ | $2.68 \mathrm{E}+02$ | $2.69 \mathrm{E}+02$ | $2.68 \mathrm{E}+02$ |
| 1323 | $2.48 \mathrm{E}+02$ | $2.45 \mathrm{E}+02$ | $2.41 \mathrm{E}+02$ | $2.45 \mathrm{E}+02$ | $2.44 \mathrm{E}+02$ | $2.41 \mathrm{E}+02$ |
| 1324 | $2.71 \mathrm{E}+02$ | $2.63 \mathrm{E}+02$ | $2.68 \mathrm{E}+02$ | $2.68 \mathrm{E}+02$ | $2.67 \mathrm{E}+02$ | $2.62 \mathrm{E}+02$ |
| 1325 | $2.75 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ | $2.69 \mathrm{E}+02$ | $2.69 \mathrm{E}+02$ | $2.74 \mathrm{E}+02$ | $2.65 \mathrm{E}+02$ |
| 1326 | $2.43 \mathrm{E}+02$ | $2.41 \mathrm{E}+02$ | $2.41 \mathrm{E}+02$ | $2.38 \mathrm{E}+02$ | $2.42 \mathrm{E}+02$ | $2.39 \mathrm{E}+02$ |
| 1327 | $2.43 \mathrm{E}+02$ | $2.42 \mathrm{E}+02$ | $2.45 \mathrm{E}+02$ | $2.45 \mathrm{E}+02$ | $2.40 \mathrm{E}+02$ | $2.40 \mathrm{E}+02$ |
| 1328 | $2.62 \mathrm{E}+02$ | $2.61 \mathrm{E}+02$ | $2.51 \mathrm{E}+02$ | $2.66 \mathrm{E}+02$ | $2.61 \mathrm{E}+02$ | $2.50 \mathrm{E}+02$ |
| 1329 | $2.41 \mathrm{E}+02$ | $2.44 \mathrm{E}+02$ | $2.44 \mathrm{E}+02$ | $2.43 \mathrm{E}+02$ | 2.39E+02 | $2.38 \mathrm{E}+02$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $2.64 \mathrm{E}+02$ | $2.59 \mathrm{E}+02$ | $2.62 \mathrm{E}+02$ | $2.63 \mathrm{E}+02$ | 2.63E+02 | $2.59 \mathrm{E}+02$ |
| Std Dev Biased | $1.32 \mathrm{E}+01$ | $1.19 \mathrm{E}+01$ | $1.31 \mathrm{E}+01$ | $1.26 \mathrm{E}+01$ | $1.28 \mathrm{E}+01$ | $1.22 \mathrm{E}+01$ |
| Ps90\%/90\% (+KTL) Biased | $3.00 \mathrm{E}+02$ | $2.92 \mathrm{E}+02$ | $2.98 \mathrm{E}+02$ | $2.98 \mathrm{E}+02$ | $2.98 \mathrm{E}+02$ | $2.93 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Biased | $2.28 \mathrm{E}+02$ | $2.27 \mathrm{E}+02$ | $2.26 \mathrm{E}+02$ | $2.29 \mathrm{E}+02$ | $2.28 \mathrm{E}+02$ | $2.26 \mathrm{E}+02$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $2.59 \mathrm{E}+02$ | $2.56 \mathrm{E}+02$ | $2.55 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.57 \mathrm{E}+02$ | $2.51 \mathrm{E}+02$ |
| Std Dev Un-Biased | $1.50 \mathrm{E}+01$ | $1.44 \mathrm{E}+01$ | $1.30 \mathrm{E}+01$ | 1.43E+01 | 1.52E+01 | $1.18 \mathrm{E}+01$ |
| Ps90\%/90\% (+KTL) Un-Biased | $3.00 \mathrm{E}+02$ | $2.96 \mathrm{E}+02$ | $2.90 \mathrm{E}+02$ | $2.96 \mathrm{E}+02$ | $2.98 \mathrm{E}+02$ | $2.84 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Un-Biased | $2.17 \mathrm{E}+02$ | $2.17 \mathrm{E}+02$ | $2.19 \mathrm{E}+02$ | $2.18 \mathrm{E}+02$ | $2.15 \mathrm{E}+02$ | $2.19 \mathrm{E}+02$ |
| Specification MIN | $1.30 \mathrm{E}+02$ | $1.30 \mathrm{E}+02$ | $1.30 \mathrm{E}+02$ | $1.30 \mathrm{E}+02$ | 1.30E+02 | $8.70 \mathrm{E}+01$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.9. Plot of Common Mode Rejection Ratio (dB) @ VS=+/-15V, VCM=+/-11V versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.9. Raw data for Common Mode Rejection Ratio (dB) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=+/-11 \mathrm{~V}$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Common Mode Rejection Ratio (dB) <br> @ VS=+/-15V, VCM=+/-11V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $9.64 \mathrm{E}+01$ | $9.61 \mathrm{E}+01$ | $9.59 \mathrm{E}+01$ | $9.58 \mathrm{E}+01$ | $9.58 \mathrm{E}+01$ | $9.58 \mathrm{E}+01$ |
| 1318 | $9.88 \mathrm{E}+01$ | $9.87 \mathrm{E}+01$ | $9.86 \mathrm{E}+01$ | $9.87 \mathrm{E}+01$ | $9.87 \mathrm{E}+01$ | $9.89 \mathrm{E}+01$ |
| 1321 | $9.02 \mathrm{E}+01$ | $9.01 \mathrm{E}+01$ | $9.01 \mathrm{E}+01$ | $9.02 \mathrm{E}+01$ | $9.02 \mathrm{E}+01$ | $9.04 \mathrm{E}+01$ |
| 1322 | $9.43 \mathrm{E}+01$ | $9.44 \mathrm{E}+01$ | $9.43 \mathrm{E}+01$ | $9.44 \mathrm{E}+01$ | $9.46 \mathrm{E}+01$ | $9.48 \mathrm{E}+01$ |
| 1323 | $9.70 \mathrm{E}+01$ | $9.68 \mathrm{E}+01$ | $9.69 \mathrm{E}+01$ | $9.69 \mathrm{E}+01$ | $9.71 \mathrm{E}+01$ | $9.76 \mathrm{E}+01$ |
| 1324 | $9.43 \mathrm{E}+01$ | $9.41 \mathrm{E}+01$ | $9.40 \mathrm{E}+01$ | $9.39 \mathrm{E}+01$ | $9.38 \mathrm{E}+01$ | $9.36 \mathrm{E}+01$ |
| 1325 | $9.06 \mathrm{E}+01$ | $9.06 \mathrm{E}+01$ | $9.05 \mathrm{E}+01$ | 9.05E+01 | $9.05 \mathrm{E}+01$ | $9.06 \mathrm{E}+01$ |
| 1326 | $9.93 \mathrm{E}+01$ | $9.92 \mathrm{E}+01$ | $9.90 \mathrm{E}+01$ | $9.88 \mathrm{E}+01$ | $9.84 \mathrm{E}+01$ | $9.85 \mathrm{E}+01$ |
| 1327 | $1.07 \mathrm{E}+02$ | $1.08 \mathrm{E}+02$ | $1.09 \mathrm{E}+02$ | $1.10 \mathrm{E}+02$ | $1.11 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ |
| 1328 | $1.01 \mathrm{E}+02$ | $1.00 \mathrm{E}+02$ | $1.00 \mathrm{E}+02$ | $9.98 \mathrm{E}+01$ | $9.93 \mathrm{E}+01$ | $9.87 \mathrm{E}+01$ |
| 1329 | $9.95 \mathrm{E}+01$ | 9.97E+01 | $9.94 \mathrm{E}+01$ | $9.95 \mathrm{E}+01$ | $9.96 \mathrm{E}+01$ | $9.94 \mathrm{E}+01$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $9.53 \mathrm{E}+01$ | 9.52E+01 | $9.52 \mathrm{E}+01$ | 9.52E+01 | $9.53 \mathrm{E}+01$ | $9.55 \mathrm{E}+01$ |
| Std Dev Biased | $3.29 \mathrm{E}+00$ | $3.25 \mathrm{E}+00$ | $3.23 \mathrm{E}+00$ | $3.21 \mathrm{E}+00$ | $3.22 \mathrm{E}+00$ | $3.26 \mathrm{E}+00$ |
| Ps $90 \% / 90 \%$ (+KTL) Biased | $1.04 \mathrm{E}+02$ | $1.04 \mathrm{E}+02$ | $1.04 \mathrm{E}+02$ | $1.04 \mathrm{E}+02$ | $1.04 \mathrm{E}+02$ | $1.04 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Biased | $8.63 \mathrm{E}+01$ | $8.63 \mathrm{E}+01$ | $8.63 \mathrm{E}+01$ | $8.64 \mathrm{E}+01$ | $8.64 \mathrm{E}+01$ | $8.66 \mathrm{E}+01$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $9.83 \mathrm{E}+01$ | $9.84 \mathrm{E}+01$ | $9.85 \mathrm{E}+01$ | $9.85 \mathrm{E}+01$ | $9.85 \mathrm{E}+01$ | $9.87 \mathrm{E}+01$ |
| Std Dev Un-Biased | $6.15 \mathrm{E}+00$ | $6.60 \mathrm{E}+00$ | $6.92 \mathrm{E}+00$ | $7.25 \mathrm{E}+00$ | $7.60 \mathrm{E}+00$ | $8.32 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Un-Biased | $1.15 \mathrm{E}+02$ | $1.17 \mathrm{E}+02$ | $1.17 \mathrm{E}+02$ | $1.18 \mathrm{E}+02$ | $1.19 \mathrm{E}+02$ | $1.22 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Un-Biased | $8.14 \mathrm{E}+01$ | $8.03 \mathrm{E}+01$ | $7.95 \mathrm{E}+01$ | $7.86 \mathrm{E}+01$ | $7.77 \mathrm{E}+01$ | $7.59 \mathrm{E}+01$ |
| Specification MIN | $8.60 \mathrm{E}+01$ | $8.60 \mathrm{E}+01$ | $8.60 \mathrm{E}+01$ | $8.60 \mathrm{E}+01$ | $8.60 \mathrm{E}+01$ | $8.60 \mathrm{E}+01$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |



Figure 5.10. Plot of Power Supply Rejection Ratio (dB) @ VS $=+/-10$ To $+/-18 \mathrm{~V}$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aleroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.10. Raw data for Power Supply Rejection Ratio (dB) @ VS=+/-10 To $+/-18 \mathrm{~V}$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Power Supply Rejection Ratio (dB) <br> @ VS=+/-10 To +/-18V | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $9.92 \mathrm{E}+01$ | $9.95 \mathrm{E}+01$ | $9.96 \mathrm{E}+01$ | $9.98 \mathrm{E}+01$ | $9.99 \mathrm{E}+01$ | $1.01 \mathrm{E}+02$ |
| 1318 | $1.01 \mathrm{E}+02$ | $1.01 \mathrm{E}+02$ | $1.01 \mathrm{E}+02$ | $1.01 \mathrm{E}+02$ | $1.01 \mathrm{E}+02$ | $1.00 \mathrm{E}+02$ |
| 1321 | $1.10 \mathrm{E}+02$ | $1.10 \mathrm{E}+02$ | $1.11 \mathrm{E}+02$ | $1.11 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ |
| 1322 | $1.20 \mathrm{E}+02$ | $1.19 \mathrm{E}+02$ | $1.19 \mathrm{E}+02$ | $1.18 \mathrm{E}+02$ | $1.16 \mathrm{E}+02$ | $1.14 \mathrm{E}+02$ |
| 1323 | $9.73 \mathrm{E}+01$ | $9.76 \mathrm{E}+01$ | $9.77 \mathrm{E}+01$ | $9.78 \mathrm{E}+01$ | $9.80 \mathrm{E}+01$ | $9.83 \mathrm{E}+01$ |
| 1324 | $9.96 \mathrm{E}+01$ | $9.98 \mathrm{E}+01$ | $9.98 \mathrm{E}+01$ | $9.99 \mathrm{E}+01$ | $1.00 \mathrm{E}+02$ | $1.00 \mathrm{E}+02$ |
| 1325 | $1.12 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.15 \mathrm{E}+02$ |
| 1326 | $1.11 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.12 \mathrm{E}+02$ | $1.14 \mathrm{E}+02$ |
| 1327 | $1.15 \mathrm{E}+02$ | $1.16 \mathrm{E}+02$ | $1.16 \mathrm{E}+02$ | 1.17E+02 | $1.17 \mathrm{E}+02$ | $1.19 \mathrm{E}+02$ |
| 1328 | $1.51 \mathrm{E}+02$ | $1.27 \mathrm{E}+02$ | $1.24 \mathrm{E}+02$ | $1.25 \mathrm{E}+02$ | $1.25 \mathrm{E}+02$ | $1.22 \mathrm{E}+02$ |
| 1329 | $1.17 \mathrm{E}+02$ | 1.17E+02 | $1.18 \mathrm{E}+02$ | $1.18 \mathrm{E}+02$ | 1.17E+02 | $1.17 \mathrm{E}+02$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $1.05 \mathrm{E}+02$ | $1.05 \mathrm{E}+02$ | $1.05 \mathrm{E}+02$ | $1.06 \mathrm{E}+02$ | $1.05 \mathrm{E}+02$ | $1.05 \mathrm{E}+02$ |
| Std Dev Biased | $9.37 \mathrm{E}+00$ | $8.90 \mathrm{E}+00$ | $8.83 \mathrm{E}+00$ | $8.82 \mathrm{E}+00$ | $8.02 \mathrm{E}+00$ | $7.71 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Biased | $1.31 \mathrm{E}+02$ | $1.30 \mathrm{E}+02$ | $1.30 \mathrm{E}+02$ | $1.30 \mathrm{E}+02$ | $1.27 \mathrm{E}+02$ | $1.26 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Biased | 7.97E+01 | $8.10 \mathrm{E}+01$ | $8.12 \mathrm{E}+01$ | 8.13E+01 | 8.32E+01 | $8.41 \mathrm{E}+01$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $1.18 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.13 \mathrm{E}+02$ | $1.14 \mathrm{E}+02$ |
| Std Dev Un-Biased | $1.95 \mathrm{E}+01$ | $9.56 \mathrm{E}+00$ | $8.72 \mathrm{E}+00$ | $9.10 \mathrm{E}+00$ | $9.17 \mathrm{E}+00$ | $8.29 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Un-Biased | $1.71 \mathrm{E}+02$ | $1.39 \mathrm{E}+02$ | $1.37 \mathrm{E}+02$ | $1.38 \mathrm{E}+02$ | $1.39 \mathrm{E}+02$ | $1.37 \mathrm{E}+02$ |
| Ps90\%/90\% (-KTL) Un-Biased | $6.43 \mathrm{E}+01$ | $8.70 \mathrm{E}+01$ | $8.90 \mathrm{E}+01$ | $8.84 \mathrm{E}+01$ | $8.83 \mathrm{E}+01$ | $9.12 \mathrm{E}+01$ |
| Specification MIN | $9.00 \mathrm{E}+01$ | $9.00 \mathrm{E}+01$ | $9.00 \mathrm{E}+01$ | $9.00 \mathrm{E}+01$ | $9.00 \mathrm{E}+01$ | $9.00 \mathrm{E}+01$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

TID Report
15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800


Figure 5.11. Plot of Positive Slew Rate ( $\mathrm{V} / \mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}$, $\mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aleroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.11. Raw data for Positive Slew Rate (V/ $\mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Positive Slew Rate (V/ Hs ) <br> @ VS=+/-15V, AV=1, RL=2k $\Omega$ | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $2.00 \mathrm{E}+01$ | $2.05 \mathrm{E}+01$ | $2.04 \mathrm{E}+01$ | $2.04 \mathrm{E}+01$ | $1.99 \mathrm{E}+01$ | $2.00 \mathrm{E}+01$ |
| 1318 | $2.15 \mathrm{E}+01$ | $2.20 \mathrm{E}+01$ | $2.19 \mathrm{E}+01$ | $2.16 \mathrm{E}+01$ | $2.14 \mathrm{E}+01$ | $2.12 \mathrm{E}+01$ |
| 1321 | $1.54 \mathrm{E}+01$ | $1.54 \mathrm{E}+01$ | $1.55 \mathrm{E}+01$ | $1.54 \mathrm{E}+01$ | $1.53 \mathrm{E}+01$ | $1.53 \mathrm{E}+01$ |
| 1322 | $1.47 \mathrm{E}+01$ | $1.44 \mathrm{E}+01$ | $1.47 \mathrm{E}+01$ | $1.46 \mathrm{E}+01$ | $1.44 \mathrm{E}+01$ | $1.45 \mathrm{E}+01$ |
| 1323 | $1.69 \mathrm{E}+01$ | $1.69 \mathrm{E}+01$ | $1.69 \mathrm{E}+01$ | $1.70 \mathrm{E}+01$ | $1.71 \mathrm{E}+01$ | $1.69 \mathrm{E}+01$ |
| 1324 | 2.08E+01 | $2.14 \mathrm{E}+01$ | $2.11 \mathrm{E}+01$ | $2.08 \mathrm{E}+01$ | 2.07E+01 | $2.04 \mathrm{E}+01$ |
| 1325 | $1.51 \mathrm{E}+01$ | $1.51 \mathrm{E}+01$ | $1.51 \mathrm{E}+01$ | $1.51 \mathrm{E}+01$ | $1.52 \mathrm{E}+01$ | $1.52 \mathrm{E}+01$ |
| 1326 | $1.52 \mathrm{E}+01$ | $1.53 \mathrm{E}+01$ | $1.54 \mathrm{E}+01$ | $1.52 \mathrm{E}+01$ | $1.53 \mathrm{E}+01$ | $1.53 \mathrm{E}+01$ |
| 1327 | $2.08 \mathrm{E}+01$ | $2.08 \mathrm{E}+01$ | $2.13 \mathrm{E}+01$ | $2.09 \mathrm{E}+01$ | $2.03 \mathrm{E}+01$ | $2.07 \mathrm{E}+01$ |
| 1328 | $2.00 \mathrm{E}+01$ | $2.08 \mathrm{E}+01$ | $2.02 \mathrm{E}+01$ | $2.04 \mathrm{E}+01$ | 2.07E+01 | $2.00 \mathrm{E}+01$ |
| 1329 | $2.07 \mathrm{E}+01$ | $2.09 \mathrm{E}+01$ | $2.10 \mathrm{E}+01$ | $2.07 \mathrm{E}+01$ | $2.07 \mathrm{E}+01$ | $2.06 \mathrm{E}+01$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $1.77 \mathrm{E}+01$ | $1.78 \mathrm{E}+01$ | $1.79 \mathrm{E}+01$ | $1.78 \mathrm{E}+01$ | $1.76 \mathrm{E}+01$ | $1.76 \mathrm{E}+01$ |
| Std Dev Biased | $2.94 \mathrm{E}+00$ | $3.26 \mathrm{E}+00$ | $3.12 \mathrm{E}+00$ | $3.09 \mathrm{E}+00$ | $2.96 \mathrm{E}+00$ | $2.93 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Biased | $2.57 \mathrm{E}+01$ | $2.68 \mathrm{E}+01$ | $2.64 \mathrm{E}+01$ | $2.63 \mathrm{E}+01$ | $2.57 \mathrm{E}+01$ | $2.56 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Biased | $9.59 \mathrm{E}+00$ | $8.88 \mathrm{E}+00$ | $9.30 \mathrm{E}+00$ | $9.34 \mathrm{E}+00$ | $9.50 \mathrm{E}+00$ | $9.56 \mathrm{E}+00$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $1.84 \mathrm{E}+01$ | $1.87 \mathrm{E}+01$ | $1.86 \mathrm{E}+01$ | $1.85 \mathrm{E}+01$ | $1.84 \mathrm{E}+01$ | $1.83 \mathrm{E}+01$ |
| Std Dev Un-Biased | $2.94 \mathrm{E}+00$ | $3.19 \mathrm{E}+00$ | $3.09 \mathrm{E}+00$ | $3.03 \mathrm{E}+00$ | $2.89 \mathrm{E}+00$ | $2.80 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Un-Biased | $2.64 \mathrm{E}+01$ | $2.74 \mathrm{E}+01$ | $2.71 \mathrm{E}+01$ | $2.68 \mathrm{E}+01$ | $2.63 \mathrm{E}+01$ | $2.60 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Un-Biased | $1.03 \mathrm{E}+01$ | $9.95 \mathrm{E}+00$ | $1.01 \mathrm{E}+01$ | $1.02 \mathrm{E}+01$ | $1.05 \mathrm{E}+01$ | $1.07 \mathrm{E}+01$ |
| Specification MIN | $1.00 \mathrm{E}+01$ | $1.00 \mathrm{E}+01$ | $1.00 \mathrm{E}+01$ | $1.00 \mathrm{E}+01$ | $9.00 \mathrm{E}+00$ | $9.00 \mathrm{E}+00$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company


Figure 5.12. Plot of Negative Slew Rate (V/ $\mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.12. Raw data for Negative Slew Rate (V/ $\mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Negative Slew Rate ( $\mathrm{V} / \mu \mathrm{s}$ ) <br> @ VS=+/-15V, AV=1, RL=2k $\Omega$ | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $-3.70 \mathrm{E}+01$ | $-3.64 \mathrm{E}+01$ | $-3.63 \mathrm{E}+01$ | $-3.62 \mathrm{E}+01$ | $-3.64 \mathrm{E}+01$ | $-3.59 \mathrm{E}+01$ |
| 1318 | $-3.83 \mathrm{E}+01$ | $-3.76 \mathrm{E}+01$ | $-3.76 \mathrm{E}+01$ | $-3.74 \mathrm{E}+01$ | $-3.75 \mathrm{E}+01$ | $-3.70 \mathrm{E}+01$ |
| 1321 | $-2.71 \mathrm{E}+01$ | $-2.70 \mathrm{E}+01$ | $-2.73 \mathrm{E}+01$ | $-2.74 \mathrm{E}+01$ | $-2.75 \mathrm{E}+01$ | $-2.70 \mathrm{E}+01$ |
| 1322 | $-2.52 \mathrm{E}+01$ | $-2.49 \mathrm{E}+01$ | $-2.54 \mathrm{E}+01$ | $-2.54 \mathrm{E}+01$ | $-2.53 \mathrm{E}+01$ | $-2.48 \mathrm{E}+01$ |
| 1323 | -2.82E+01 | $-2.82 \mathrm{E}+01$ | $-2.83 \mathrm{E}+01$ | $-2.87 \mathrm{E}+01$ | $-2.87 \mathrm{E}+01$ | $-2.85 \mathrm{E}+01$ |
| 1324 | $-3.76 \mathrm{E}+01$ | $-3.72 \mathrm{E}+01$ | $-3.73 E+01$ | $-3.71 \mathrm{E}+01$ | $-3.68 \mathrm{E}+01$ | $-3.70 \mathrm{E}+01$ |
| 1325 | $-2.54 \mathrm{E}+01$ | $-2.53 \mathrm{E}+01$ | $-2.54 \mathrm{E}+01$ | $-2.57 \mathrm{E}+01$ | $-2.58 \mathrm{E}+01$ | $-2.55 \mathrm{E}+01$ |
| 1326 | -2.69E+01 | $-2.68 \mathrm{E}+01$ | $-2.70 \mathrm{E}+01$ | $-2.72 \mathrm{E}+01$ | $-2.73 \mathrm{E}+01$ | $-2.71 \mathrm{E}+01$ |
| 1327 | $-3.95 \mathrm{E}+01$ | $-3.94 \mathrm{E}+01$ | $-3.92 \mathrm{E}+01$ | $-3.92 \mathrm{E}+01$ | $-3.93 \mathrm{E}+01$ | $-3.95 \mathrm{E}+01$ |
| 1328 | $-3.79 \mathrm{E}+01$ | $-3.74 \mathrm{E}+01$ | $-3.70 \mathrm{E}+01$ | $-3.73 \mathrm{E}+01$ | $-3.72 \mathrm{E}+01$ | $-3.75 \mathrm{E}+01$ |
| 1329 | -3.94E+01 | $-3.97 \mathrm{E}+01$ | $-3.96 \mathrm{E}+01$ | $-3.96 \mathrm{E}+01$ | -3.95E+01 | $-3.95 \mathrm{E}+01$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $-3.12 \mathrm{E}+01$ | $-3.08 \mathrm{E}+01$ | $-3.10 \mathrm{E}+01$ | $-3.10 \mathrm{E}+01$ | $-3.11 \mathrm{E}+01$ | $-3.06 \mathrm{E}+01$ |
| Std Dev Biased | $6.06 \mathrm{E}+00$ | $5.79 \mathrm{E}+00$ | $5.54 \mathrm{E}+00$ | $5.41 \mathrm{E}+00$ | $5.48 \mathrm{E}+00$ | $5.46 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Biased | $-1.45 \mathrm{E}+01$ | $-1.50 \mathrm{E}+01$ | $-1.58 \mathrm{E}+01$ | $-1.62 \mathrm{E}+01$ | $-1.61 \mathrm{E}+01$ | $-1.57 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Biased | $-4.78 \mathrm{E}+01$ | -4.67E+01 | -4.62E+01 | -4.59E+01 | -4.61E+01 | $-4.56 \mathrm{E}+01$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $-3.35 \mathrm{E}+01$ | $-3.32 \mathrm{E}+01$ | $-3.32 \mathrm{E}+01$ | $-3.33 \mathrm{E}+01$ | $-3.33 \mathrm{E}+01$ | -3.33E+01 |
| Std Dev Un-Biased | $6.73 \mathrm{E}+00$ | $6.65 \mathrm{E}+00$ | $6.45 \mathrm{E}+00$ | $6.34 \mathrm{E}+00$ | $6.27 \mathrm{E}+00$ | $6.51 \mathrm{E}+00$ |
| Ps90\%/90\% (+KTL) Un-Biased | $-1.50 \mathrm{E}+01$ | $-1.50 \mathrm{E}+01$ | $-1.55 \mathrm{E}+01$ | $-1.59 \mathrm{E}+01$ | $-1.61 \mathrm{E}+01$ | $-1.55 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Un-Biased | $-5.19 \mathrm{E}+01$ | $-5.14 \mathrm{E}+01$ | $-5.09 \mathrm{E}+01$ | $-5.07 \mathrm{E}+01$ | $-5.05 \mathrm{E}+01$ | $-5.12 \mathrm{E}+01$ |
| Specification MAX | -1.00E+01 | -1.00E+01 | -1.00E+01 | -1.00E+01 | $-9.00 \mathrm{E}+00$ | $-9.00 \mathrm{E}+00$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company


Figure 5.13. Plot of Positive Output Voltage Swing (V) @ VS $=+/-15 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex
Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.13. Raw data for Positive Output Voltage Swing (V) @ VS $=+/-15 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Positive Output Voltage Swing (V) <br> @ VS=+/-15V, RL=2k $\Omega$ | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1318 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1321 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1322 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1323 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1324 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1325 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1326 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1327 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1328 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| 1329 | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Std Dev Biased | 3.70E-03 | $3.91 \mathrm{E}-03$ | 3.05E-03 | $3.51 \mathrm{E}-03$ | $4.04 \mathrm{E}-03$ | $4.27 \mathrm{E}-03$ |
| Ps90\%/90\% (+KTL) Biased | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Biased | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Std Dev Un-Biased | $2.17 \mathrm{E}-03$ | $2.05 \mathrm{E}-03$ | 3.36E-03 | 1.82E-03 | $1.52 \mathrm{E}-03$ | $2.00 \mathrm{E}-03$ |
| Ps90\%/90\% (+KTL) Un-Biased | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Un-Biased | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ | $1.32 \mathrm{E}+01$ |
| Specification MIN | $1.20 \mathrm{E}+01$ | $1.20 \mathrm{E}+01$ | $1.20 \mathrm{E}+01$ | $1.20 \mathrm{E}+01$ | $1.20 \mathrm{E}+01$ | $1.20 \mathrm{E}+01$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company


Figure 5.14. Plot of Negative Output Voltage Swing (V) @ VS=+/-15V, RL=2k $\Omega$ versus total dose. The solid diamonds are the average of the measured data points for the samples irradiated under electrical bias while the shaded diamonds are the average of the measured data points for the samples irradiated with all pins tied to ground. The black lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated under electrical bias while the gray lines (solid and/or dashed) are the upper and/or lower confidence limits, as determined by KTL statistics, on the samples irradiated in the unbiased condition. The red dotted line(s) are the pre- and/or post-irradiation minimum and/or maximum specification value as defined in the datasheet and/or test plan.

## TID Report <br> 15-0704 07/12/16 R1.1

Aleroflex

Aeroflex RAD
5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table 5.14. Raw data for Negative Output Voltage Swing (V) @ VS $=+/-15 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ versus total dose, including the statistical analysis, specification and the status of the testing (pass/fail).

| Negative Output Voltage Swing (V) @ VS=+/-15V, RL=2k | Total Dose (krad(Si)) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Device | 0 | 10 | 20 | 30 | 50 | 100 |
| 1317 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| 1318 | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 E+01$ |
| 1321 | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| 1322 | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 E+01$ |
| 1323 | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| 1324 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 E+01$ |
| 1325 | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| 1326 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 E+01$ |
| 1327 | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| 1328 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 E+01$ |
| 1329 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| Biased Statistics |  |  |  |  |  |  |
| Average Biased | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | -1.31E+01 | $-1.31 \mathrm{E}+01$ |
| Std Dev Biased | 1.16E-02 | 1.11E-02 | $1.40 \mathrm{E}-02$ | 1.32E-02 | 1.31E-02 | $1.59 \mathrm{E}-02$ |
| Ps90\%/90\% (+KTL) Biased | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.30 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Biased | -1.31E+01 | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| Un-Biased Statistics |  |  |  |  |  |  |
| Average Un-Biased | -1.31E+01 | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| Std Dev Un-Biased | 1.69E-02 | $1.56 \mathrm{E}-02$ | 1.70E-02 | $1.68 \mathrm{E}-02$ | 1.83E-02 | $2.07 \mathrm{E}-02$ |
| Ps90\%/90\% (+KTL) Un-Biased | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ | $-1.30 \mathrm{E}+01$ |
| Ps90\%/90\% (-KTL) Un-Biased | $-1.32 \mathrm{E}+01$ | -1.32E+01 | $-1.32 \mathrm{E}+01$ | $-1.32 \mathrm{E}+01$ | $-1.32 \mathrm{E}+01$ | $-1.31 \mathrm{E}+01$ |
| Specification MAX | -1.20E+01 | -1.20E+01 | $-1.20 \mathrm{E}+01$ | $-1.20 \mathrm{E}+01$ | $-1.20 \mathrm{E}+01$ | $-1.20 E+01$ |
| Status | PASS | PASS | PASS | PASS | PASS | PASS |

An ISO 9001:2008 and DLA Certified Company

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

### 6.0. Summary / Conclusions

The total ionizing dose testing described in this final report was performed using the facilities at Aeroflex RAD's Longmire Laboratories in Colorado Springs, CO. The high dose rate total ionizing dose (TID) source is a JLSA 81-24 irradiator modified to provide a panoramic exposure. The Co-60 rods are held in the base of the irradiator heavily shielded by lead, during the radiation exposures the rod is raised by an electronic timer/controller and the exposure is performed in air. The dose rate for this irradiator in this configuration ranges from <1rad(Si)/s to a maximum of approximately $300 \mathrm{rad}(\mathrm{Si}) / \mathrm{s}$, determined by the distance from the source.

The parametric data was obtained as "read and record" and all the raw data plus an attributes summary are contained in this report as well as in a separate Excel file. The attributes data contains the average, standard deviation and the average with the KTL values applied. The KTL value used in this work is 2.742 per MIL-HDBK-814 using one sided tolerance limits of $90 / 90$ and a 5-piece sample size. The 90/90 KTL values were selected to match the statistical levels specified in the MIL-PRF-38535 sampling plan for the qualification of a radiation hardness assured (RHA) component. Note that the following criteria must be met for a device to pass the total ionizing dose test: following the radiation exposure each of the 5 pieces irradiated under electrical bias shall pass the specification value. The units irradiated without electrical bias and the KTL statistics are included in this report for reference only. If any of the 5 pieces irradiated under electrical bias exceed the device post radiation data sheet specification limits, then the lot could be logged as a failure.

Based on this criterion the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier (from the lot date code identified on the first page of this test report) PASSED the total ionizing dose test to the maximum tested dose level of $100 \mathrm{krad}(\mathrm{Si})$ with all parameters remaining within their datasheet specifications. Further, the data in this report can be analyzed along with the low dose rate report titled "Enhanced Low Dose Rate Sensitivity (ELDRS) Radiation Testing of the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier for Linear Technology" to demonstrate that these parts do not exhibit ELDRS as defined in the current test method.

Aleroflex

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Appendix A: Photograph of Packing Label and a Sample Unit-Under-Test to Show Part Traceability


An ISO 9001:2008 and DLA Certified Company

## Appendix B: Radiation Bias Connections and Absolute Maximum Ratings

TID Radiation Biased Conditions: Supplied by Aeroflex-RAD.

| Pin | Function | Connection / Bias |
| :--- | :--- | :--- |
| 1 | NC | NC |
| 2 | BAL | NC |
| 3 | - IN | To Pin 7 via $10 \mathrm{k} \Omega$ Resister |
| 4 | + IN | To 8 V via $10 \mathrm{k} \Omega$ Resister |
| 5 | V- | To -15 V Decoupled to GND W/ $0.1 \mu \mathrm{~F}$ Capacitor |
| 6 | BAL | NC |
| 7 | OUT | To Pin 3 via $10 \mathrm{k} \Omega$ Resister |
| 8 | V+ | To +15 V Decoupled to GND W/ $0.1 \mu \mathrm{~F}$ Capacitor |
| 9 | NC | NC |
| 10 | NC | NC |



Figure B.1. Irradiation bias circuit.

TID Radiation Unbiased Conditions: All pins grounded.

| Pin | Function | Connection / Bias |
| :--- | :--- | :--- |
| 1 | NC | GND |
| 2 | BAL | GND |
| 3 | -IN | GND |
| 4 | + IN | GND |
| 5 | V- | GND |
| 6 | BAL | GND |
| 7 | OUT | GND |
| 8 | V+ | GND |
| 9 | NC | GND |
| 10 | NC | GND |



Figure B.2. W package drawing (for reference only). This figure was extracted from Linear Technology RH1056A Datasheet ID No. 66-10-0160 Rev C.

## Absolute Maximum Ratings:

| Parameter | Max Rating |
| :--- | :--- |
| Supply Voltage | $\pm 20 \mathrm{~V}$ |
| Differential Input Voltage | $\pm 40 \mathrm{~V}$ |
| Input Voltage | $\pm 20 \mathrm{~V}$ |
| Output Short-Circuit Duration | Indefinite |

## TID Report 15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

## Appendix C: Electrical Test Parameters and Conditions

The expected ranges of values as well as the measurement conditions are taken from Linear Technology RH1056A Datasheet ID No. 66-10-0160 Rev C. All electrical tests for this device are performed on one of Aeroflex RAD's LTS2020 Test Systems. The LTS2020 Test System is a programmable parametric tester that provides parameter measurements for a variety of digital, analog and mixed signal products including voltage regulators, voltage comparators, D to A and A to D converters. The LTS2020 Test System achieves accuracy and sensitivity through the use of software self-calibration and an internal relay matrix with separate family boards and custom personality adapter boards. The tester uses this relay matrix to connect the required test circuits, select the appropriate voltage / current sources and establish the needed measurement loops for all the tests performed. The measured parameters and test conditions are shown in Table C.1.

A listing of the measurement precision/resolution for each parameter is shown in Table C.2. The precision/resolution values were obtained from test data or from the DAC resolution of the LTS-2020 for the particular test shown, whichever is greater. To generate the precision/resolution shown in Table C.2, one of the units-under-test was tested repetitively (a total of 10-times with re-insertion between tests) to obtain the average test value and standard deviation. Using this test data MIL-HDBK-814 90/90 KTL statistics were applied to the measured standard deviation to generate the final measurement range. This value encompasses the precision/resolution of all aspects of the test system, including the LTS2020 mainframe, family board, socket assembly and DUT board as well as insertion error. In some cases, the measurement resolution is limited by the internal DACs, which results in a measured standard deviation of zero. In these instances the precision/resolution will be reported back as the LSB of the DAC.

Note that the testing and statistics used in this document are based on an "analysis of variables" technique, which relies on small sample sizes to qualify much larger lot sizes (see MIL-HDBK-814, p. 91 for a discussion of statistical treatments). Not all measured parameters are well suited to this approach due to inherent large variations. If necessary, larger samples sizes could be used to qualify these parameters using an "attributes" approach.

## TID Report <br> 15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

Table C.1. Measured parameters and test conditions for the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier.

| Parameter | Symbol | Test Conditions |
| :--- | :--- | :--- |
| Positive Supply Current (A) | + IS | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ |
| Negative Supply Current (A) | -IS | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ |
| Input Offset Voltage (V) | VOS | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ |
| Input Offset Current (A) | IOS | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ |
| Positive Input Bias Current (A) | +IB | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ |
| Negative Input Bias Current (A) | -IB | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$ |
| Large Signal Voltage Gain1 (V/mV) | AVOL1 | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VO}=+/-10 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ |
| Large Signal Voltage Gain2 (V/mV) | AVOL2 | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VO}=+/-10 \mathrm{~V}, \mathrm{RL}=1 \mathrm{k} \Omega$ |
| Common Mode Rejection Ratio (dB) | CMRR | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{VCM}=+/-11 \mathrm{~V}$ |
| Power Supply Rejection Ratio (dB) | PSRR | $\mathrm{VS}=+/-10 \mathrm{To}+/-18 \mathrm{~V}$ |
| Positive Slew Rate (V/ $\mu \mathrm{s}$ ) | +SR | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$ |
| Negative Slew Rate (V/ $\mu \mathrm{s}$ ) | -SR | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$ |
| Positive Output Voltage Swing (V) | +VOUT | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ |
| Negative Output Voltage Swing (V) | -VOUT | $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$ |

## TID Report 15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial Blvd. Colorado Springs, CO 80919 (719) 531-0800

Table C.2. Measured parameters, pre-irradiation specifications and measurement precision for the RH1056AMW Precision, High Speed, JFET Input Operational Amplifier.

| Parameter | Pre-Irradiation Specification |  | Measurement Precision/Resolution |
| :--- | :---: | :---: | :---: |
|  | MIN | MAX |  |
| Positive Supply Current (A) |  | $6.50 \mathrm{E}-03$ | $\pm 2.14 \mathrm{E}-05$ |
| Negative Supply Current (A) | $-6.50 \mathrm{E}-03$ |  | $\pm 2.49 \mathrm{E}-05$ |
| Input Offset Voltage (V) | $-3.00 \mathrm{E}-04$ | $3.00 \mathrm{E}-04$ | $\pm 3.83 \mathrm{E}-06$ |
| Input Offset Current (A) | $-1.00 \mathrm{E}-11$ | $1.00 \mathrm{E}-11$ | $\pm 7.15 \mathrm{E}-13$ |
| Positive Input Bias Current (A) | $-5.00 \mathrm{E}-11$ | $5.00 \mathrm{E}-11$ | $\pm 1.59 \mathrm{E}-12$ |
| Negative Input Bias Current (A) | $-5.00 \mathrm{E}-11$ | $5.00 \mathrm{E}-11$ | $\pm 1.43 \mathrm{E}-12$ |
| Large Signal Voltage Gain1 (V/mV) | $1.50 \mathrm{E}+02$ |  | $\pm 5.04 \mathrm{E}+00 \%$ |
| Large Signal Voltage Gain2 (V/mV) | $1.30 \mathrm{E}+02$ |  | $\pm 4.98 \mathrm{E}+00 \%$ |
| Common Mode Rejection Ratio (dB) | $8.60 \mathrm{E}+01$ |  | $\pm 4.11 \mathrm{E}+00$ |
| Power Supply Rejection Ratio (dB) | $9.00 \mathrm{E}+01$ |  | $\pm 1.44 \mathrm{E}-01$ |
| Positive Slew Rate (V/ $\mu \mathrm{s})$ | $1.00 \mathrm{E}+01$ |  | $\pm 3.51 \mathrm{E}-01$ |
| Negative Slew Rate (V/ $\mu \mathrm{s}$ ) |  | $-1.00 \mathrm{E}+01$ | $\pm 4.31 \mathrm{E}-01$ |
| Positive Output Voltage Swing (V) | $1.20 \mathrm{E}+01$ |  | $\pm 3.90 \mathrm{E}-03$ |
| Negative Output Voltage Swing (V) |  | $-1.20 \mathrm{E}+01$ | $\pm 1.02 \mathrm{E}-02$ |

TID Report
15-0704 07/12/16 R1.1

Aeroflex RAD 5030 Centennial BIvd. Colorado Springs, CO 80919 (719) 531-0800

## Appendix D: List of Figures Used in the Results Section (Section 5)

5.1. Positive Supply Current (A) @ VS=+/-15V, VCM=0V
5.2. Negative Supply Current (A) @ VS=+/-15V, VCM=0V
5.3. Input Offset Voltage (V) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$
5.4. Input Offset Current (A) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=0 \mathrm{~V}$
5.5. Positive Input Bias Current (A) @ VS=+/-15V, VCM=0V
5.6. Negative Input Bias Current (A) @ VS=+/-15V, VCM=0V
5.7. Large Signal Voltage Gain1 (V/mV) @ VS=+/-15V, VO =+/-10V, RL=2k $\Omega$
5.8. Large Signal Voltage Gain2 (V/mV) @ VS $=+/-15 \mathrm{~V}, \mathrm{VO}=+/-10 \mathrm{~V}, \mathrm{RL}=1 \mathrm{k} \Omega$
5.9. Common Mode Rejection Ratio (dB) @ VS $=+/-15 \mathrm{~V}, \mathrm{VCM}=+/-11 \mathrm{~V}$
5.10. Power Supply Rejection Ratio (dB) @ VS=+/-10 To +/-18V
5.11. Positive Slew Rate $(\mathrm{V} / \mu \mathrm{s})$ @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$
5.12. Negative Slew Rate (V/ $\mu \mathrm{s}$ ) @ $\mathrm{VS}=+/-15 \mathrm{~V}, \mathrm{AV}=1, \mathrm{RL}=2 \mathrm{k} \Omega$
5.13. Positive Output Voltage Swing (V) @ VS=+/-15V, RL=2k $\Omega$
5.14. Negative Output Voltage Swing (V) @ VS $=+/-15 \mathrm{~V}, \mathrm{RL}=2 \mathrm{k} \Omega$

