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AC ANALOG VOLTMETERS

by Harry Logan

AC Analog voltmeters are one of the most popular electronic measuring instruments in use today. They are used to measure the RMS voltage of the many waveforms commonly found in electronics.

This article will provide you with the basics of AC analog voltmeters. It will give you a better understanding of their operation, allowing you to select the right one for your particular measurement.

The RMS or root-mean-square voltage is measured because this value gives us the most information about the waveform. The RMS voltage is equivalent to a DC voltage which produces the same heating effect as the AC signal being measured. For example, 1 volt of DC across a 1 ohm resistor will dissipate 1 watt. If we substitute any periodic waveform in place of the DC source and adjust its amplitude so that we again have 1 watt of power dissipated in the load,

then our AC signal has an RMS or effective value of 1 volt.

In addition to its RMS value, a waveform also has a peak and average voltage value. See Figure 1.

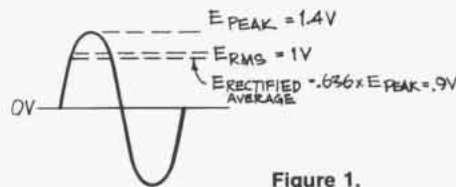


Figure 1.

This sine wave has an RMS value of 1 volt. Its peak value is 1.4 times its RMS value, or 1.4 volts. Its rectified average or DC value is .636 times the peak or .9 volts in the above example.

AC voltmeters are designed to respond to one of these three values. This classifies the meters into *true RMS* responding, *average* responding and *peak* responding. The average and peak responding voltmeters are designed to measure only sine waves.

Average Responding

With an average responding voltmeter, a sine wave being measured is fed through a DC blocking capacitor,

amplified or attenuated, rectified by the diode bridge and fed to the meter. The meter then responds to this rectified average or DC value.

The average value of a sine wave is zero, so when we say average responding we mean the rectified average or DC component after rectification. This DC component deflects a d'Arsonval (moving coil) meter to indicate the RMS value of a sine wave. See Figure 2.

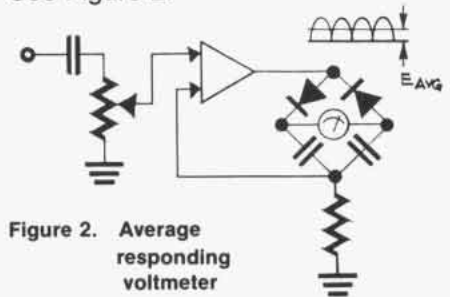


Figure 2. Average responding voltmeter

The average responding meter is the most popular and economical type of AC voltmeter. Its voltage scale has been made to indicate the RMS value of a sine wave. If any other waveform is measured, the meter will read incorrectly. Typical average responding voltmeters are the HP 400 D/H/L, 403A/B and 400E/EL.



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Peak Responding

Peak responding voltmeters are also designed to indicate the RMS value of a sine wave.

A capacitor in the probe charges through a rectifying diode to the positive peak of the applied sine wave. The voltmeter then responds to the DC output from the probe.

The peak responding meter has its rectifier in the probe instead of inside the voltmeter, so we convert from AC to DC as close to the signal as possible. Because the cable carries DC only, cable capacity does not affect the measurement. This greatly increases the high frequency response of the instrument. See Figure 3.

The AC probe can be switched out of the circuit and the voltmeter can then be used to measure DC voltages. By adding shunt resistors and an internal

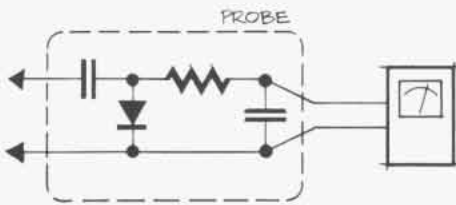


Figure 3. Peak responding voltmeters

DC voltage source, we can also measure current and resistance. Typical peak responding voltmeters are the HP 410B and 410C.

RMS Responding

True RMS voltmeters are unique because they are the only type that accurately measure non-sinesoidal waveforms. They respond to the RMS or heating value of the impressed signal. See Figure 4.

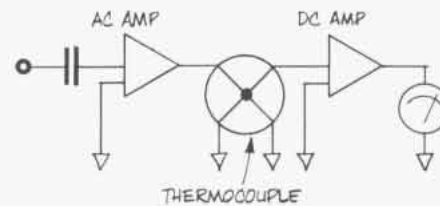


Figure 4. True RMS voltmeter

The input signal is AC coupled, amplified or attenuated and heats a thermocouple. The thermocouple produces a DC output proportional to the RMS value of the AC input. This DC voltage is amplified and deflects the meter needle to the RMS value. The response of the thermocouple is not dependent on the waveshape and thus true RMS voltmeters can accurately measure non-sinesoidal waveforms.

A limitation on the waveforms that can

be measured with a true RMS voltmeter is crest factor. Crest factor must be considered when measuring pulse type signals — signals with a high peak and low RMS voltage. Crest factor is defined in terms of duty cycle or as the peak voltage divided by the RMS voltage. See Figure 5.

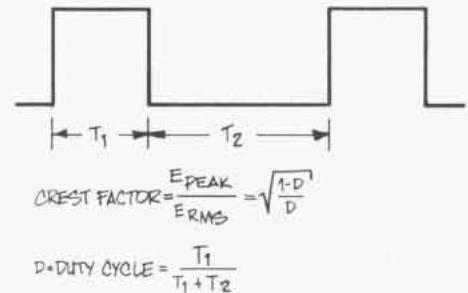


Figure 5. Crest factor



Figure 6.

The pulse in Figure 6 has a crest factor of 8. To measure it accurately, a true RMS Voltmeter with a specified crest factor of at least 8 is required. Crest factor limitation of a voltmeter is determined by its dynamic range. For example, because the pulse in Figure 6 has

RMS VOLTAGE

RMS stands for root-mean-square. We can use this definition to calculate the RMS or heating value of any waveform. Let's apply it to the 10v p-p square wave of Figure A. This will give us an insight into the meaning of RMS.



Figure A.

Applying the definition of RMS, we take the square root of the average value squared.

$$E_{RMS} = \sqrt{(E_{AVERAGE})^2 \frac{1}{2} \text{cycle} + (E_{AVERAGE})^2 \frac{1}{2} \text{cycle}} = \sqrt{(5)^2 \frac{1}{2} + (5)^2 \frac{1}{2}} = \sqrt{25} = 5v \text{ RMS}$$



Figure B.

Now suppose our 10v p-p square wave looked like the one in Figure B. Does it have the same RMS value as

the square wave of Figure A? Note that the waveform is not symmetrical around 0v or ground. This means the waveform has a DC component, +5v in this case. So we really have two signals, +5v DC and a 10v p-p square wave superimposed on it. The square wave in Figure A has no DC component. Therefore the square wave of Figure B must have a greater RMS value. Again applying the definition of RMS we get:

$$E_{RMS} = \sqrt{(10)^2 \frac{1}{2} + (0)^2 \frac{1}{2}} = \sqrt{50} = 7.07v$$

Most true RMS voltmeters are AC coupled and would block the +5v DC component, thus measuring only the RMS value of the square wave. So when measuring any non-symmetrical waveform (one with a DC component), we must measure both the AC and DC components separately and use this formula:

$$E_{RMS} = \sqrt{DC^2 + AC^2}$$

For the waveform of Figure B we would get:

$$E_{RMS} = \sqrt{5^2 + 5^2} = \sqrt{50} = 7.07$$

This is the same value as was obtained applying the definition of RMS.

an RMS value of 1 volt, we should measure it on the 1 volt range. But the voltmeter's amplifier must also be able to handle the 8 volt level without saturation even though we're on the one volt range.

Of course, true RMS voltmeters can also measure sine waves since their crest factor is only 1.4. See Figure 7.

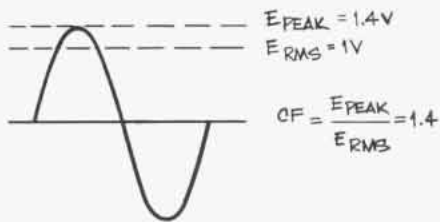


Figure 7.

Typical true RMS voltmeters are the HP 3400A, 3403C, 3480/3484A and 3450A/B.

Distortion Effects

All three types of meters will read correctly with a sine wave. With a distorted sine wave, only the true RMS meter will read correctly. The average responding and peak responding meters will be in error.

Table 1 lists the inaccuracies resulting from distortion. The table shows that a given amount of harmonic distortion may result in a wide range of possible inaccuracies, a consequence of the fact that the phase as well as the amplitude of a harmonic component affects the readings. This is illustrated by Figure 8, which shows two waveforms both with identical amounts of fundamental frequency and added 3rd harmonic. In the diagram at left, the fundamental crosses the zero baseline in phase with the harmonic waveform and in the diagram at right they are out of phase.

The peak responding meter would show a range of readings between "a"

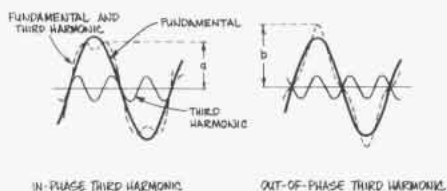


Figure 8. Phase of harmonics in waveform affect shape and thus the peak value of a complex wave.

| HARMONIC CONTENT | TRUE RMS VALUE (VOLTS) | AVERAGE RESPONDING METER (VOLTS) | PEAK RESPONDING METER (VOLTS) |
|------------------|------------------------|----------------------------------|-------------------------------|
| 0 | 100 | 100 | 100 |
| 10 percent 2nd | 100.5 | 100 | 90 to 110 |
| 20 percent 2nd | 102 | 100-102 | 80 to 120 |
| 50 percent 2nd | 112 | 100-110 | 75 to 150 |
| 10 percent 3rd | 100.5 | 96-104 | 90 to 110 |
| 20 percent 3rd | 102 | 94-108 | 88 to 120 |
| 50 percent 3rd | 112 | 90-116 | 108 to 150 |

Table 1. Measurement errors from harmonic voltages.

and "b", depending upon the phase of the harmonic. The range of amplitudes that would be shown by the average responding meter is more difficult to diagnose, but note that in the left diagram two half-cycles of the third harmonic add to the fundamental while one half-cycle subtracts whereas in the right diagram, only one half-cycle adds while two half-cycles subtract. The waveform in the right diagram therefore has a lower average value than the left waveform.

Thus, the desired accuracy in the measurement determines the amount of distortion, (meaning departure from true sine wave), that can be tolerated in the measured waveform. The RMS voltmeter is unaffected by waveform shapes excepting, of course, those cases when harmonic components lie outside the passband of the voltmeter circuits or beyond the crest factor.

The RMS responding meter is especially useful, for example, in the monitoring of the line power fed to a resistive load where the line regulator distorts the waveform; another application is measurement of the frequency response of a communication system, where modulation and demodulation processes may be non-linear to an unknown degree. Again, the average responding meter tolerates relatively large amounts of distortion, while the peak responding meter is most sensitive to distortion.

Voltmeter Accuracy

The accuracy of AC voltmeters is often specified as a percentage of full scale. For example, if our voltmeter is specified as 1% of full scale and we are on the 100 volt range, any measurement would be in error by $\pm 1\%$ of 100 volts

or ± 1 volt. If the input signal were 10 volts, it would be measured with ± 1 volt, an accuracy of $\pm 10\%$ of our reading. However, by downranging to the 10 volt range, the measurement can be made to $\pm 1\%$ of reading. For greatest accuracy, we should make our measurements as close as possible to full scale.

There are other items that contribute to total error. Refer to the operating manual for your voltmeter's accuracy specifications.

AC Measurements with a DC Component

Another accuracy consideration when using AC voltmeters is whether the signal contains a DC component. For example, if we wanted to measure the power dissipation in the load resistor in Figure 9, we must consider both the AC and DC voltage components.

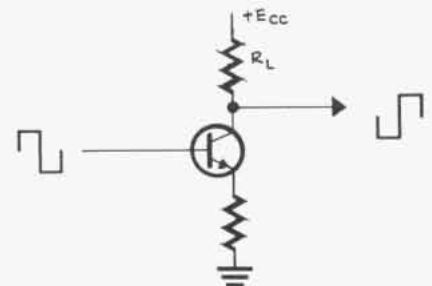


Figure 9.

Since the AC signal is a square wave, we have to use a true RMS voltmeter to measure its RMS value. However, most meters are AC coupled so the DC component is blocked. We must include this DC portion of our signal to get the total power dissipation. A DC voltmeter must be used to measure the DC component. The RMS value of the waveform can then be calculated using both meter readings and

the formula: $E_{RMS} = \sqrt{(DC)^2 + (AC)^2}$

The trend in voltmeters is toward digital readouts. Some digital voltmeters can be direct coupled when measuring an AC signal with a DC component. This allows you to make the above measurement without any calculations.

SUMMARY AND HINTS

1. Peak and average responding AC voltmeters accurately measure pure sine waves only. The more we deviate from a pure sine wave, the greater the error. Peak responding are affected the most by distortion. As a rule of thumb, average responding meters can tolerate up to 10% harmonic distortion and peak responding 5%. True

RMS meters are unaffected by distortion.

2. RMS voltage is measured because it gives us the most information about the waveform; it is equivalent to a DC voltage which produces the same heating effect as the AC being measured.

3. For a quick workbench check of your AC voltmeter, you can use your scope's square wave calibrator output. For a 1v peak to peak signal, the true RMS meter will read 0.5v; the average responding 0.55v and the peak responding 0.35v.

4. Peak responding voltmeters can measure the highest frequencies, typically up to 0.5 to 1 GHz.

5. If you measure pulses, know the

crest factor limitation of your voltmeter.

6. Any time you measure a signal that is non-symmetrical, you must measure both the AC and DC components and compute the RMS value from this formula:

$$E_{RMS} = \sqrt{(DC)^2 + (AC)^2}$$

7. For maximum accuracy, use your voltmeter as close as possible to full-scale deflection.

Reference material for the article included HP Application Note 60 "Which AC Voltmeter;" HP Application Note 124 "True RMS Measurements;" and HP Videotape No. 90030B Opt. 605, "Choosing the Right AC Voltmeter."

SCALE FACTORS

The reason peak and average responding voltmeters are accurate only on sine waves is because of the scale factors designed into them. Consider the waveform in Figure A. An RMS responding voltmeter will measure the true RMS value of 10 V and it will deflect the meter to 10 v (that is, its scale factor is exactly 1.0). A peak responding meter will respond to the 14 v peak but will apply a scale factor of 0.707, and therefore it will also deflect its meter to the desired 10 volts reading, ($14 \times 0.707 = 10$). An average responding meter

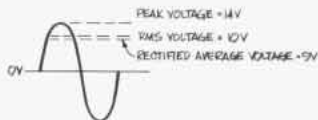


Figure A. 10V RMS Sine wave



Figure B. 10V Square wave

will respond to the 9 v rectified average value and multiply by its scale factor of 1.11 to read 10 volts. Therefore all three meters read 10v for this sine wave, which is correct.

Consider now the waveform in Figure B. An RMS responding meter will measure and display 10 v, which is the correct RMS voltage for this waveform. A peak responding meter will respond to the 10 v peak but *will still apply the correction factor for a sine wave of 0.707* and thus display 7.07 v. An average responding voltmeter will respond to the rectified average of 10 v but it will also apply its scale factor for a sine wave of 1.11, displaying 11.1 v.

Since peak and average responding voltmeters are designed to measure sine waves, each has a scale factor for sine waves. Measuring any other wave shape requires a different scale factor and therefore these meters read incorrectly.



Harry Logan is currently working in HP Corporate Television producing several new video tapes. He joined the Company eight years ago and has spent most of that time in the Training Department teaching customers and HP personnel on low frequency instrumentation.

Harry is an avid photography enthusiast; he enjoys woodworking and gardening, in addition to playing the accordion and organ.



REPLACEMENT PART CROSS REFERENCE

When selecting replacement parts for your HP products, you may notice that many manuals list only an HP part number for the part, even though it appears that this part is manufactured by one of the large semiconductor manufacturers. Service personnel often ask why only HP part numbers are listed.

It is recommended that HP replacement parts be used to ensure that the original performance of the product will be obtained. While some parts used in HP instruments are identical to that which can be purchased at a local electronics distributor, many times parts will be selected for certain characteristics, such as gain, bandwidth, ca-

pacitance, etc. There may also be slight mechanical differences, such as the shaping or length of leads. In some cases special quality checks are employed to ensure that high reliability parts are used at the factory and at HP field offices.

Therefore, we suggest obtaining replacement parts from HP to maintain the quality that you have paid for in your instrument. There may be situations however where HP replacement parts are not in stock and substituting parts will allow you to return the product to service immediately. In these cases it may be worthwhile to see if a

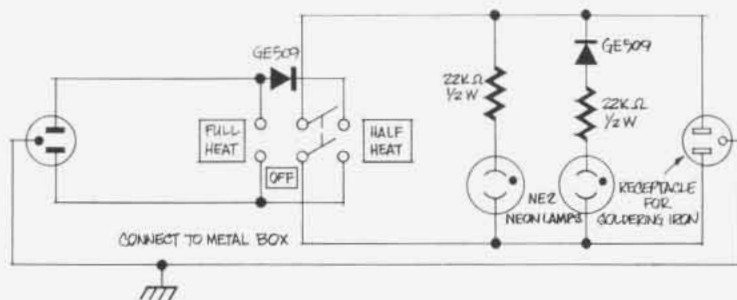
substitute part will work in the circuit. Perhaps an HP part could be ordered and installed at some later date.

To help you in these situations, here's a cross-reference of HP part numbers to JEDEC numbers for transistors and diodes, plus a listing of manufacturer and manufacturers' part numbers for ICs. While every attempt was made to ensure the accuracy of the list, it is advisable to compare the description of the device being replaced with the description of the substituted part. For example, if the service manual describes the device being replaced as a "dual J-K flip-flop", check this against the description of the replacement part.

| HP P/N | JEDEC NO. | | | | | | | | |
|-----------|------------|-----------|-----------|-----------|--------------|-----------|-------------|-----------|------------|
| 0122-0004 | -- 1N4809 | 1A50-0096 | -- 2N2189 | 1A51-0025 | -- 2N1706 | 1A53-0310 | -- 2N4398 | 1A54-0214 | -- 2N1482 |
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| 1A50-0073 | -- 2N1204 | 1A50-0405 | -- 2N1215 | 1A53-0221 | -- 2N5416 | 1A54-0092 | -- *2N3563 | 1A54-0363 | -- 2N5262 |
| 1A50-0074 | -- 2N1396 | 1A50-0406 | -- 2N1760 | 1A53-0222 | -- 2N4919 | 1A54-0093 | -- 2N3415 | 1A54-0365 | -- *2N4410 |
| 1A50-0075 | -- 2N779A | 1A50-0409 | -- 2N2644 | 1A53-0223 | -- 2N4902 | 1A54-0094 | -- *2N3646 | 1A54-0368 | -- 2N5191 |
| 1A50-0076 | -- 2N2556 | 1A50-0412 | -- *2N270 | 1A53-0236 | -- 2N5193 | 1A54-0096 | -- 2N3405 | 1A54-0370 | -- 2N5294 |
| 1A50-0082 | -- 2N1363 | 1A50-0414 | -- 2N1703 | 1A53-0258 | -- 2N4035 | 1A54-0098 | -- 2N3392 | 1A54-0371 | -- *2N3391 |
| 1A50-0087 | -- 2N1544 | 1A50-0417 | -- 2N597 | 1A53-0264 | -- *2N5401 | 1A54-0099 | -- *2N3393 | 1A54-0378 | -- 2N5109 |
| 1A50-0090 | -- 2N1183B | 1A50-0418 | -- 2N600 | 1A53-0269 | -- 2N3809 | 1A54-0201 | -- *2N3391A | 1A54-0379 | -- 2N4298 |
| 1A50-0091 | -- 2N2048 | 1A50-0419 | -- 2N2707 | 1A53-0277 | -- 2N5954 | 1A54-0202 | -- *2N3390 | 1A54-0382 | -- 2N4348 |
| 1A50-0092 | -- 2N2043 | 1A50-0431 | -- 2N4277 | 1A53-0280 | -- 2N5195 | 1A54-0203 | -- *2N3694 | 1A54-0384 | -- 2N5184 |
| 1A50-0093 | -- 2N1499A | 1A50-0437 | -- 2N2872 | 1A53-0281 | -- 2N2907A | 1A54-0209 | -- 2N510 | 1A54-0386 | -- 2N5070 |
| 1A50-0094 | -- 2N1360 | 1A50-0438 | -- 2N208A | 1A53-0285 | -- *2N3638 | 1A54-0210 | -- 2N2222 | 1A54-0389 | -- 2N4922 |
| 1A50-0095 | -- 2N297A | 1A51-0006 | -- 2N169A | 1A53-0293 | -- 2N5583 | 1A54-0211 | -- 2N2501 | 1A54-0390 | -- 2N5181 |
| | | 1A51-0017 | -- 2N1704 | 1A53-0303 | -- 2N5956 | 1A54-0212 | -- 2N2897 | 1A54-0392 | -- *2N5088 |
| | | 1A51-0024 | -- 2N388A | 1A53-0305 | -- 2N5875 | 1A54-0213 | -- 2N2538 | 1A54-0397 | -- 2N4996 |

SOLDERING IRON TIP SAVER

by Bryson Nishimura and Michael A. Caughey



Here is a simple but very useful gadget that makes your solder iron more useful in addition to extending the life of the tips.

The materials needed are:

- interlocking chassis 4" × 2¼" × 2¼"
- silicon rectifier 1A 400V
- DPDT - Center off switch 3A 125vac
- misc. - plugs, outlet, wire, grommet

Total parts cost, which is about \$4.00, may be reduced by using locally available parts, since parts selection is not critical. Construction is easy and should require about an hour. Layout is not critical, but care should be taken to maintain adequate spacing of all leads from the metal box. Using a three wire cord is recommended since this allows grounding of the metal box. Neon lamps can be added as shown in the schematic for visual indication of full or half heat. One lamp lights for half heat and both light for full heat.

Operation of the tip saver is simple. When the switch is placed in the position without the diode, full line voltage is connected to the solder iron and full temperature is reached. This is useful for fast warmup in the morning and for soldering tasks where a large amount of heat is needed, such as large chassis ground connections or ground planes on a P.C. board.

When the diode is switched in the circuit, the effective voltage is cut in half and the temperature is therefore also reduced. This prevents overheating of the tip when the solder iron is not being used. This half-heat position also works well for soldering and unsoldering IC's, transistors, diodes, etc. where high temperatures are undesirable.

Having a three position center off switch makes a convenient method of turning off the solder iron at night, rather than unplugging it as was done previously.

We use the Ungar 777 iron with a 1235 element and PL333 tip in most of our applications. We have been using the tip saver in our Calibration Lab and other shops now for about two years and the results are very good. In one case, a tip lasted about 14 months without replacement even though it was on all day, five days a week. This has resulted in considerable savings.

Editor's Note: A number of methods can be used to vary solder iron power, including several available commercially.

Additional control would be possible with a design using a triac and potentiometer, (or using a variable line voltage control available on many service benches). Many people feel that the simple circuit above is sufficient, however. Your comments are invited.

Bryson Nishimura has been with the Hawaiian Telephone Company in Honolulu for 4 years, working as a Calibration Laboratory Technician. This entails repair and calibration of about 400 different models of test equipment. He attended the Electronics Institute of Hawaii. As might be expected of someone from Hawaii, Bryson enjoys surfing, as well as photography.

Michael A. Caughey is the Electronic Shop Supervisor at the Hawaiian Telephone Company. This shop is a repair facility for multiplex carrier and traffic data systems. Michael received his electronics training at the Navy Electronics School and he also is a part-time student at the University of Hawaii. In addition to photography, his outside interests include automobile rallying.

THE CONTRIBUTIONS OF EDESEL MURPHY TO THE UNDERSTANDING OF THE BEHAVIOR OF INANIMATE OBJECTS

Readers may be familiar with an oft quoted basic principle called Murphy's Law. This states that "If anything can go wrong, it will."

Some time ago, samples of the application of this principle were printed in EDN/EEE, an electronics publication intended for design engineers. For your enjoyment, some of these are reprinted here, courtesy of EDN/EEE.



General Engineering

- Dimensions will always be expressed in the least usable term. Velocity, for example, will be expressed in furlongs per fortnight.
- An important Instruction Manual or Operating Manual will have been discarded by the Receiving Department.

Prototyping and Production

- Any wire cut to length will be too short.
- Tolerances will accumulate unidirectionally toward maximum difficulty of assembly.
- Identical units tested under identical conditions will not be identical in the field.
- The availability of a component is inversely proportional to the need for the component.
 - If a project requires n components, there will be n-1 units in stock.
 - If a particular resistance is needed, that value will not be available. Further, it cannot be developed with any available series or parallel combination.
 - A dropped tool will land where it can do the most damage. (Also known as the law of selective gravitation.)
 - The probability of a dimension being omitted from a plan or drawing is proportional to its importance.

- Interchangeable parts won't.
- Probability of failure of a component, assembly, subsystem or system is inversely proportional to ease of repair or replacement.
- If a prototype functions perfectly, subsequent production units will malfunction.
- Components that must not and cannot be assembled improperly will be.
- Graphic recorders will deposit

more ink on humans than on paper.

- An instantaneous power-supply crowbar circuit will operate too late.
- A transistor protected by a fast-acting fuse will protect the fuse by blowing first.
- If an obviously defective component is replaced in an instrument with an intermittent fault, the fault will reappear after the instrument is returned to service.

● After the last of 16 mounting screws has been removed from an access cover, it will be discovered that the wrong access cover has been removed.

● After an access cover has been secured by 16 hold-down screws, it will be discovered that the gasket has been omitted.

● After an instrument has been fully assembled, extra components will be found on the bench.

PLOTTER HAVE THE JITTERS?

by Vern Hudson

A symptom of jitters in X-Y plotters or strip chart recorders is one that sometimes causes consternation. The pen will appear jumpy or noisy in a certain position. This erratic operation can be repeated by using the zero control or signal input to move the pen to the erratic position.

The solution is to clean the slide wire, the variable resistor in the feedback loop that determines the position of the pen. The slidewire should be cleaned with a cotton swab moistened with freon degreaser.

After cleaning the slidewire, which is a precision resistor, be sure to lubricate it to ensure proper operation and normal life. It is *extremely* important to use the correct lubricant.

The majority of HP plotters have a wirewound slidewire; these need slidewire lubricant HP p/n 5080-3635.

Many of the new plotters, such as the 7123-7143 series, have a film slidewire mixed in with a plastic base. This looks something like a composition resistor. Film slidewires require grease that can be obtained by ordering HP p/n 07143-69134.

Wirewound and film slidewires each have a unique appearance that makes them easily distinguishable.

If the plotter is in daily use, HP recommends cleaning the slidewire once each month. After cleaning, the standard calibration procedure should be used to verify proper operation. Refer to the service manual of your instrument for details.

A CLEAN HEAD HELPS



Many people using analog or digital tape recorders are surprised to learn that the heads should be cleaned before *each* use.

As the tape passes over a head, two things happen that are detrimental to performance: The tape slowly wears metal away from the head and oxide from the tape is deposited on the head.

As the oxide coating increases in thickness, the separation between tape and head increases, reducing the high frequency response and degrading the signal to noise ratio. If further oxide build-up is allowed, it causes increased and irregular tape wear, which causes increased oxide deposits, etc.

To keep this from happening to your tape recorder, clean the heads before each use with cotton swabs and Freon TF Degreaser. Moisten the cotton with freon and wipe the tape head with a sideways motion. It is important that the heads be wiped in the *same direction that the tape travels*. Continue this process, using several additional clean cotton swabs, until no more oxide is visible on the cotton.

Often times the oxide on a head is not easily visible. I once repaired a unit

that had one channel dead. The customer insisted that he had cleaned the heads and they indeed looked clean. Examination under a microscope showed a substantial oxide layer that was the cause of his problem. This was removed by scrubbing with the freon.

Freon degreaser is commonly available in liquid or spray form. Liquid freon tape head cleaner is available from HP under p/n 8500-1251. Cotton swabs mounted on a thin wooden stick can be purchased locally or ordered through HP p/n 8520-0023. Care must be taken to avoid excessive freon in the tape recorder. Do not apply freon directly to the head; moisten the cotton swab and then gently wipe the head.

Clean heads and proper preventive maintenance procedures help you retain the performance designed into your recorder. Refer to the maintenance section of your manual for details of these procedures.

Editor's note: This procedure is also a good idea for your home stereo recorder, if you happen to be a stereophonic sound enthusiast.

Vern Hudson has been with HP for fourteen years, working initially on a production line, testing finished products. He soon moved to the repair bench at the HP Customer Service Center in Mountain View, California, servicing recorders and printers.

He recently accepted a position at the San Diego (California) Division of HP, working as a Service Engineer. Vern is one of the product experts that provide technical assistance to the HP Field Service Organization.



NEW
SERVICE NOTES
NEW VIDEOTAPES
NEW PRODUCTS
NEW DEVICES
BOOKS

When a lot of fine people work together something good usually happens. This aptly describes the story of Bench Briefs, since this publication relies on participation from you, the reader. While stopping to reflect on the past year, it became evident that a large number of people have helped make a successful year for Bench Briefs. I would like to extend my thanks and Christmas wishes to all of you.

The most visible group on any publication is the people writing articles. Contributing Editors and Contributing Authors involved during 1973 were Rod Dinkins, Chris Franks, Marv Willrodt, George Stanley, Dan Struckmann, Harry Logan, Vern Hudson, Bryson Nishimura and Michael Caughey. Bryson and Michael are with the Hawaiian Telephone Company. All others are with H.P.

The difference between a Contributing Editor and Author is the degree of involvement. A Contributing Editor is a person selected at an HP facility to regularly coordinate Bench Briefs activities and to submit articles for publication. A Contributing Author can be anyone from any company with a suitable article.

In addition to the people writing material, there are a great number of additional people involved in making Bench Briefs possible and I would like to take this opportunity to express my thanks and best wishes.

After the material is written for an issue, it must be prepared for the printing process, then printed and distributed.

Gary Welden of The Graphic Circle has been a great help with the planning, design, and graphics. Many of his ideas are evident in each issue. The cartoon illustrations have been the work of Vance Locke, of Vance Locke Illustrations, Budd Cady and Roy Anderson. Typing has been done by Dolores Owen, Donnita Arnold and Barb Cummins. Photo type-setting is the work of Anne LoPresti and Jodi Montgomery. Hal Netten provided editorial assistance.

Printing has been handled very well by Bruce Woodd of the National Press. In fact, Bruce and his people have occasionally worked remarkably fast to ensure that Bench Briefs was mailed on schedule.

Distribution of the printed copies is a very important area and there are many people working behind-the-scenes who share in this Christmas Greeting. Doris Brunelli and Jim Kinney keep the mailing list current and Les Considine of Coast Mailing Corporation handles the addressing and mailing of Bench Briefs. Distribution to HP factories and offices is handled by Gloria Frazier and Walt Cavaness. Requests for Service Notes are also handled by Walt and he is assisted by Eleanor Jimenez. Peter Tacx directs distribution of Bench Briefs and Service Notes for Europe. Peter is located in Amsterdam.

And, of course, I would be remiss to neglect mentioning you, the reader, without whom all of the above would be unnecessary.

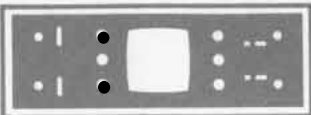
I wish all of you a very special and joyous Merry Christmas.

Have a challenging and prosperous New Year.

Dick Gasperini
Editor



NEW TOOLS
MORE SERVICE TIPS
TUTORIAL ARTICLES
APPLICATION NOTES
MODIFICATIONS
ADJUSTMENTS



MODIFICATIONS

5326/5327 SERIES UNIVERSAL COUNTER MODIFICATIONS

A modification for the 5326/5327 series Universal Counters is recommended to improve reliability of the power supplies. This is done by adding two transistor insulators to the series regulator transistor for the +5 and -5 volt power supplies.

This change applies to instruments with these serial numbers and below:

| Model | Serial Number |
|-------|---------------|
| 5326A | 1312A 02005 |
| 5326B | 1312A 02265 |
| 5326C | 1312A 00500 |
| 5327A | 1312A 00410 |
| 5327B | 1312A 00620 |
| 5327C | 1312A 00595 |

The parts required are -

| Item | HP-P/N |
|--------------------------|-----------|
| Kapton Insulator- 2 Each | 0340-0765 |
| #8 Washer - 2 Each | 3050-0001 |
| Bushing - 2 Each | 1200-0081 |
| Heat Sink Compound | 8500-0269 |

When ordering the parts, request Service Note 5326A/B/C/5327A/B/C-4. This gives details and the installation procedure.

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READER COMMENTS OR TECHNICAL ARTICLE CONTRIBUTIONS ARE WELCOMED. PLEASE SEND THEM TO THE ABOVE ADDRESS.

| | |
|-----------------------|--|
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