

Analog Engineer's Circuit: Amplifiers SNOAA02-August 2018

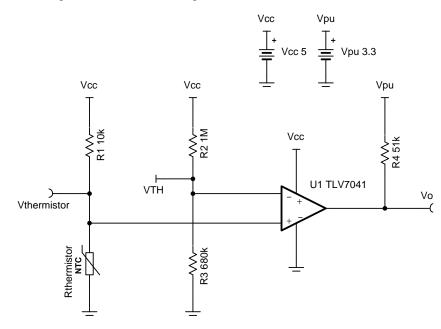
# Thermal switch circuit

### **Design Goals**

Temperature Switching Point	Output		Supply		
T <sub>sp</sub>	$V_o = HIGH$	$V_o = LOW$	V <sub>cc</sub>	V <sub>ee</sub>	V <sub>pu</sub>
100 °C	$T_A < T_{sp}$	$T_A > T_{sp}$	5V	0V	3.3V

### **Design Description**

This thermal switch solution will signal low (to a GPIO pin) when a certain temperature is exceeded thus alerting when conditions are no longer optimal or device-safe. This circuit incorporates an NTC thermistor with a comparator configured in a non-inverting fashion.



### **Design Notes**

- 1. The resistance of an NTC thermistor drops as temperature increases.
- 2. The TLV7041 has an open drain output, so a pull-up resistor is required.
- 3. Configurations where the thermistor is placed near the high side of the divider can be done; however, the comparator will have to be used in an inverting fashion to still have the output switch low.
- 4. To exercise good practice, a positive feedback resistor should be placed to add external hysteresis (for simplicity, it is not done in this example).

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#### **Design Steps**

 Select an NTC thermistor, preferably one with a high nominal resistance, R<sub>0</sub>, (resistance value when ambient temperature, T<sub>A</sub>, is 25 °C) since the TLV7041 has a very low input bias current. This will help lower power consumption, thus reducing the likelihood of reading a slightly higher temperature due to thermal dissipation in the thermistor. The thermistor chosen has its R<sub>0</sub> and its material constant, β, listed below.

 $R_0 = 100 k\Omega$ 

- $\beta = 3977 K$
- Select R<sub>1</sub>. For high temperature switching points, R<sub>1</sub> should be 10 times smaller than the nominal resistance of the thermistor. This causes a larger voltage difference per temperature change around the temperature switching point, which helps guarantee the output will switch at the desired temperature value.

$$\begin{split} R_1 &= \frac{R_0}{10} \\ R_1 &= \frac{100 k\Omega}{10} = 10 k\Omega \ \ (\text{Standard Value}) \end{split}$$

3. Select  $R_2$ . Again, this can be a high resistance value.

 $R_2 = 1M\Omega$  (Standard Value)

4. Solve for the resistance of the thermistor, R<sub>thermistor</sub>, at the desired temperature switching point. Using the  $\beta$  formula is an effective approximation for thermistor resistance across the temperature range of -20 °C to 120 °C. Alternatively, the Steinhart-Hart equation can be used, but several device-specific constants must be provided by the thermistor vendor. Note that temperature values are in Kelvin. Here T<sub>0</sub> = 25 °C = 298.15K.

$$\mathsf{R}_{\text{thermistor}}(\mathsf{T}_{\text{sp}}) = \mathsf{R}_{0} \times e^{\beta \times \left(\frac{1}{\mathsf{T}_{\text{sp}}} - \frac{1}{\mathsf{T}_{0}}\right)}$$

$$R_{thermistor}(100^{\circ}C) = 100k\Omega \times e^{3977K \times \left(\frac{1}{373.15K} - \frac{1}{298.15K}\right)}$$

 $R_{thermistor}(100^{\circ}C) = 6.85 \text{ k}\Omega$ 

5. Solve for V<sub>thermistor</sub> at T<sub>sp</sub>.

$$\begin{split} V_{thermistor}(T_{sp}) &= V_{cc} \star \frac{R_{thermistor}(T_{sp})}{R_1 + R_{thermistor}(T_{sp})} \\ V_{thermistor}(100^{\circ}C) &= 5V \star \frac{6.85 k\Omega}{10 k\Omega + 6.85 k\Omega} = 2.03V \end{split}$$

6. Solve for  $R_3$  with the threshold voltage,  $V_{TH}$ , equal to  $V_{thermistor}$ . This ensures that  $V_{thermistor}$  will always be larger than  $V_{TH}$  until the temperature switching point is exceeded.

$$\begin{split} \mathsf{R}_3 &= \frac{\mathsf{R}_2 \times \mathsf{V}_{\mathsf{TH}}}{\mathsf{V}_{\mathsf{cc}} - \mathsf{V}_{\mathsf{TH}}} \\ \mathsf{R}_3 &= \frac{\mathsf{1}\mathsf{M}\Omega \times 2.03\mathsf{V}}{\mathsf{5}\mathsf{V} - 2.03\mathsf{V}} = 685\mathsf{k}\Omega \\ \mathsf{R}_3 &= 680\mathsf{k}\Omega \quad \text{(Standard Value)} \end{split}$$

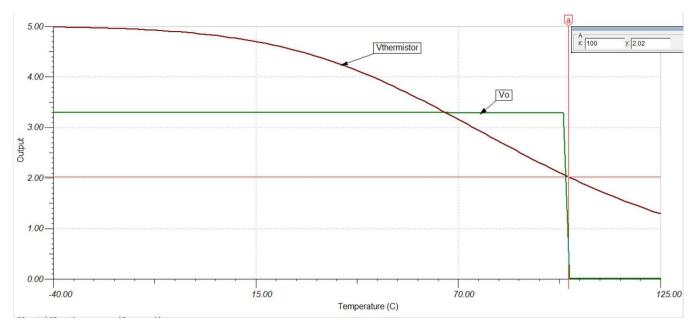
- 7. Select an appropriate pull up resistor,  $R_4$ . Here,  $V_{pu} = 3.3V$  (digital high for a microcontroller).
  - $R_4 = 51k\Omega$  (Standard Value)



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## **Design Simulations**

# **DC Temperature Simulation Results**



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# **Design References**

See Analog Engineer's Circuit Cookbooks for TI's comprehensive circuit library.

See Circuit SPICE Simulation File SLVMCS1, www.ti.com/lit/zip/slvmcs1.

## **Design Featured Comparator**

TLV7041			
Output Type	Open-Drain		
V <sub>cc</sub>	1.6V to 6.5V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>os</sub>	±100µV		
V <sub>HYS</sub>	7mV		
Ι <sub>q</sub>	335nA/Ch		
t <sub>pd</sub>	3µs		
#Channels	1		
www.ti.com/product/tlv7041			

# **Design Alternate Comparator**

TLV1701			
Output Type	Open-Collector		
V <sub>cc</sub>	2.2V to 36V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>os</sub>	±500µV		
V <sub>HYS</sub>	N/A		
l <sub>q</sub>	55µA/Ch		
t <sub>pd</sub>	560ns		
#Channels	1, 2, 4		
	www.ti.com/product/tlv1701		
	www.ti.com/product/tlv1701-q1		

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