

Technical documentation

[TPS8804](https://www.ti.com/product/TPS8804) [SLVSF29C](https://www.ti.com/lit/pdf/SLVSF29) – OCTOBER 2019 – REVISED AUGUST 2021

TPS8804 Smoke Detector AFE

1 Features

Texas

• Photo Chamber AFE

INSTRUMENTS

- Dual 8-bit programmable current LED drivers
- Temperature compensation of LED current
- Ultra-low offset op-amp for photodiodes
- Programmable and bypassable gain stage
- Carbon Monoxide Sensor AFE
	- Ultra-low offset gain stage
	- Programmable gain and reference
- Power Management
	- Programmable LDO for external microcontroller
- SLC interface transmitter and receiver
- Ultra-low power consumption
- I²C serial interface
- Wide input voltage range

2 Applications

Smoke and CO detector

3 Description

The TPS8804 integrates all of the amplifiers and drivers required for a dual-wave photoelectric smoke detection and carbon monoxide detection system. Its high flexibility is ideal for smoke detection systems where precision and power consumption are critical.

Device Information(1)

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Simplified Application

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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

5 Pin Configuration and Functions

Pin Functions

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6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)

(1) Stresses beyond those listed under *Absolute Maximum Rating* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Condition*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

6.2 ESD Ratings

over operating free-air temperature range (unless otherwise noted)

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

¹ JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

² JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](http://www.ti.com/lit/pdf/spra953) application report.

6.5 Electrical Characteristics

(1) MCU LDO output voltage on power-up is determined by the MCUSEL pin state.

6.6 Typical Characteristics

 $T_A = 27$ °C, VCC = 3.65 V

7 Detailed Description

7.1 Overview

The TPS8804 integrates an analog supply LDO, digital supply LDO, photoelectric chamber analog front end (AFE), carbon monoxide sensor AFE, SLC interface driver, analog multiplexer, and digital core. The high integration greatly reduces component count in smoke detectors and carbon monoxide detectors. The two LED drivers have highly configurable temperature compensation to support IR and blue LEDs over a wide range of currents. The wide bandwidth of the photo-amplifier saves power due to reduced LED on-time. The CO amplifier has integrated gain resistors. The SLC interface driver connects to the two-wire power line, driving it low and sensing when the line has been pulled low. Each block is highly configurable with the digital core I²C interface, supporting on-the-fly adjustment of amplifier gains, regulator voltages, and driver currents. Configurable status and interrupt signal registers alert the MCU of fault conditions such as under-voltage, over-temperature, and SLC power alerts.

7.2 Functional Block Diagram

7.3 Feature Description

7.3.1 System Power-up

Figure 7-1. Power-up State Diagram

The TPS8804 can power-up from a DC power supply above 3.6 V connected to the VCC pin. When the VCC voltage exceeds the V_{PWRIP} threshold, the TPS8804 initializes for 6 ms. After the initialization, the MCUSEL pin is sensed for 2 ms to determine the MCULDO voltage and program the VMCUSET register. Table 7-1 indicates the VMCU setting for each MCUSEL configuration. The MCULDO is enabled and the system waits for VMCU to reach its power-good threshold (typically 85% of its target voltage). It is only after VMCU reaches its power-good threshold that I2C communication is allowed with the TPS8804. This sequence of events is outlined in Figure 7-1.

MCUSEL Connection	VMCU (V)
$620 - \Omega$ to GND	1.5
Short to GND	18
Short to VINT	25
330-pF to GND	33

Table 7-1. VMCU Power-up Voltage

7.3.2 LDO Regulators

7.3.2.1 Power LDO Regulator

The power LDO is a voltage clamp that supplies many of the internal blocks in the TPS8804, including the internal LDO and MCU LDO. Because the power LDO is designed to clamp the VCC voltage, it is not precise and varies with VCC voltage and load. The power LDO shorts VCC and PLDO when the VCC voltage is below approximately 5 V, and regulates VCC when VCC is above approximately 5 V. The power LDO has a dropout voltage of approximately 1 V when it is regulating VCC. When the power LDO transitions from shorting to regulating, the PLDO voltage drops by approximately 1 V. Connect a 1-µF capacitor to PLDO to stabilize the PLDO voltage.

The power LDO is designed for use by the device and can be used to supply external circuitry that has a voltage limit of 7 V. The power LDO can also be used to supply the IR or blue LED anode through a diode.

7.3.2.2 Internal LDO Regulator

The internal LDO (INT LDO) regulator powers the TPS8804 amplifiers and digital core with a stable 2.3 V supply. Connect a 1-µF capacitor to VINT to stabilize the output. The INT LDO is always enabled when the device is powered. The INT LDO can be used to supply external circuitry. It is not recommended to power noisy or

switching loads with INT LDO, as any noise on VINT couples to the internal amplifiers and can generate noise. The INT LDO can be used in the CO connectivity test circuitry and the photo reference circuitry.

7.3.2.3 Microcontroller LDO Regulator

The microcontroller LDO (MCU LDO) powers the internal digital input and output buffers (IO buffers) and external MCU that controls and programs the TPS8804. Connect a 1-µF capacitor to VMCU to stabilize the output. The MCU LDO can be programmed to output 1.5 V, 1.8 V, 2.5 V, and 3.3 V. The default MCU LDO setting is determined by the configuration on the MCUSEL pin (see [Table 7-1](#page-18-0)). After the device is powered, the MCU LDO voltage can be changed using the VMCUSET register. The MCU LDO can also be disabled using the MCU_DIS register.

The MCU LDO output VMCU powers the IO buffers on SCL, SDA, CSEL, GPIO, LEDEN, MCU_RX, MCU_TX1, MCU TX2. The IO buffers level shift signals from the digital core to a level suitable for the microcontroller and signals from the microcontroller to a level suitable for the digital core. In general, connect VMCU to the microcontroller supply voltage to guarantee logic level compatibility. If the MCU LDO is disabled, connect an external supply to VMCU.

The MCU LDO has a power good signal MCU_PG that indicates whether the MCU LDO is above 85% the regulation voltage. A 125-µs deglitch filter prevents noise from affecting the MCU_PG signal. If MCU_PG is low after 10 ms of changing the MCU LDO voltage or enabling the MCU LDO, the MCU_ERR flag is set high. If the MCU_ERR flag is high and MCUERR_DIS is low, the MCU LDO fault state is entered. See [Section 7.4.1.1](#page-28-0) section for more information.

7.3.3 Photo Chamber AFE

Figure 7-2. Photo Amplifier Circuit

The TPS8804 photo amplifier connects to a photoelectric chamber photodiode and has two stages—an input stage and gain stage. When the photoelectric chamber LED is enabled, light scatters off smoke particles in the chamber into the photodiode, producing a signal proportional to the smoke concentration. The output of each photo amplifier stage is connected to the AMUX for ADC reading. This configuration provides high bandwidth and dynamic range for the photodiode signal chain as the gain stage is on-the-fly adjustable.

7.3.3.1 Photo Input Amplifier

The input stage is a wide-bandwidth, low-offset op-amp designed for amplifying photodiode currents. In [Figure](#page-19-0) [7-2](#page-19-0), negative feedback causes the photodiode to conduct with zero voltage bias. The photo-current flows through resistors connected from PDP to a reference (GND or PREF) and PDN to PDO. These two resistors determine the gain of the input stage. The same value must be used for these two resistors because PDP and PDN leakage is amplified by these resistors. Capacitors installed in parallel with the resistors compensate the op-amp feedback loop for optimal response. The optimal compensation capacitance depends on the photodiode's capacitance. The compensation capacitance should be adjusted to minimize settling time without having overshoot on the output of the amplifier. Overshoot adds unnecessary noise in the output. The input stage outputs through the PDO pin, which is internally connected to the integrated photo gain stage and AMUX.

The input stage has the option of being referenced to GND or PREF. PREF is a reference that is normally pulled to VINT and is set to 50 mV when PREF_SEL = 1 and either PAMP_EN = 1 or PGAIN_EN = 1. The 50 mV reference keeps the input amplifier in a linear operating region when no signal is applied, improving the speed and zero-current sensitivity of the amplifier. It is generally recommended to set PREF_SEL=1 and connect the external gain resistor and compensation capacitor to PREF. Connect a 100-pF filtering capacitor from PREF to GND to reduce high frequency noise on PREF.

When measuring the photo amplifier output, it is recommended to take multiple ADC samples. Averaging ADC samples approximately reduces the noise by the square root of the amount of samples. The power consumed in a photoelectric smoke measurement is dominated by the LED power consumption, which is proportional to the LED on-time multiplied by the LED current. To maximize the signal-to-noise ratio for a given power level, set the LED pulse length to approximately twice the photo amplifier rise time and take multiple ADC samples while the output is stabilized.

In systems where the compensation capacitor is selected for a slower rise time and lower noise, take multiple ADC samples around the peak of the photo amplifier output.

7.3.3.2 Photo Gain Amplifier

The high-bandwidth, low noise photo gain amplifier connects to the output of the photo input stage to further amplify the photodiode signal. The gain amplifier is adjustable on-the-fly using the I^2C interface. The gain amplifier has four settings:

- 5x (4.75x if PREF_SEL=1)
- 11x (10.4x if PREF_SEL=1)
- 20x (18.5x if PREF_SEL=1)
- 35x (32.3x if PREF_SEL=1)

The gain stage has the option of being referenced to GND or PREF with the PREF SEL bit. When PREF_SEL=1, a 5 mV reference offset counteracts the gain stage's input offset voltage to keep the gain stage output above 50 mV. The 5 mV reference offset is amplified by the gain stage, causing the output to change when the gain is changed, even when there is zero photo-current. It is recommended to connect a 470 kΩ resistor from PREF to VINT if the gain is set to 11x, 20x, or 35x. This resistor changes the PREF voltage to 70 mV and prevents the output from dropping below 50 mV in worst-case conditions. Referencing the gain stage to PREF causes the 50 mV reference to change with signal level due to the finite impedance of the reference. Because the reference is changing with the signal level, the gain is slightly less with PREF SEL=1.

7.3.4 LED Driver

Figure 7-3. LED Driver Circuit

7.3.4.1 LED Current Sink

The two LED drivers are current regulated, temperature compensated, and adjustable with an 8-bit DAC. When the LED driver is enabled, the CSA voltage is regulated, and the current through the CSA resistor also flows through the LED and the DINA pin. A current sense resistor connects to the CSA pin. The LED driver is enabled with the LEDEN pin and LEDPIN EN bit. Both the pin and bit must be high for the LED driver to operate. The LEDSEL bit switches which driver the LEDEN signal connects to. The GPIO pin can be configured to enable either LED driver.

The LED driver is temperature compensated to account for reduced LED intensity with increasing temperature. Four temperature compensation settings are available to support a variety of IR and blue LEDs. Temperature compensation is implemented by varying the CSA regulated voltage with temperature, thus the temperature compensation also depends on the CSA resistor. Each temperature compensation setting has a different DAC output at room temperature. To achieve a specific temperature compensation and current, the PDAC, TEMPCO, and CSA resistor must all be adjusted according to the [Section 8.2.2.2](#page-39-0) procedure.

The two LED drivers are interchangeable and support both IR and blue LEDs. The only difference between the two LED drivers is a code CSA_BIN available to improve the LED A driver current accuracy for IR LEDs. CSA_BIN in register 0x00 categorizes CSA voltage for each unit as close to the minimum, below average, above average, or close to the maximum (see [Section 7.6\)](#page-29-0). Use CSA_BIN to adjust the DAC and compensate for the variation on the LED A driver's current. After adjusting the DAC, the effective variation is reduced by a factor of 4 for the TEMPCOA = 11, PDAC $A = 00$ setting. IR LEDs typically require the TEMPCOA = 11 temperature compensation setting. Therefore, use the LED driver A for powering IR LEDs. If better accuracy is required,

calibrate the LED driver current by connecting the CSA or CSB pin to the microcontroller ADC port, measuring the CSA or CSB voltage, and adjusting PDAC_A or PDAC_B until the required current is achieved.

Ensure that the LED current remains below 550 mA, the pulse width remains below 1 ms, and the duty cycle remains below 1%. There is no protection to prevent operation outside these conditions. Ensure the PDAC and TEMPCO registers are programmed before enabling the LED driver.

7.3.4.2 LED Voltage Supply

Enough voltage must be provided to the LED such that the DINA voltage is at least the dropout voltage (V_{DINA,DROP}) above the CSA voltage while the LED driver is enabled. Ensure the DINA voltage does not exceed 11.5 V. Because of the high LED drive currents, a large capacitor connected to the LED anode is required to provide pulsed power to the LED. Any of the internal regulators (PLDO, LEDLDO) or external supply (VDC) meeting the voltage requirements can be used to charge the LED capacitor. Connect the LED anode to LEDLDO when VCC > 11.5 V.

The LED LDO clamps the VSLC voltage and blocks reverse current with an integrated diode. It is current limited to prevent inrush current caused by charging the large capacitor. The regulation voltage is adjustable in the LEDLDO register. The LED LDO may be operated with VSLC below the regulation voltage. In this case, the LEDLDO voltage stabilizes to VSLC minus a diode voltage drop.

The LED driver current and rise time can vary by a few millivolts and microseconds across the LED anode supply and VCC voltages. It is recommended to use a consistent LED anode voltage whenever the LED driver is enabled.

Connect a capacitor with a value between 1 µF and 100 µF to the LEDLDO.

7.3.5 Carbon Monoxide Sensor AFE

Figure 7-4. Carbon Monoxide Detection Circuit Referenced to GND

Figure 7-5. Carbon Monoxide Detection Circuit Referenced to 300mV

The TPS8804 CO AFE connects to an electrochemical CO sensor. The amplifier converts the microamps of sensor current into a voltage readable by an ADC. This is achieved with a low-offset, low-power op-amp with configurable input, gain, and output resistors.

7.3.5.1 CO Transimpedance Amplifier

The CO transimpedance amplifier is a low-offset, low-power op-amp with integrated input, gain, and output resistors. Each of these resistors can be disconnected using the COSW register bits if using external resistors. The input resistor limits amplifier current during a CO sensor connectivity test. The gain resistor amplifies the CO sensor signal. Adjust the gain resistor by changing the COGAIN register bits. Use the output resistor with an external capacitor to filter the CO amplifier output signal.

The CO amplifier has two integrated references. A programmable 1.25-mV to 5-mV reference COREF is internally connected to the op-amp positive terminal. A 300-mV reference is connected to the REF0P3 pin. When the millivolt reference is used, the CO sensor must be connected to GND. The millivolt reference is amplified to offset the amplifier output above GND. When the 300 mV reference is used, the reference offsets the CO amplifier output by 300 mV. In general, either reference can be used. The 300-mV reference offers better DC accuracy at the cost of extra power consumption. The 300 mV reference is generated with a reference and op-amp buffer for high precision. The REF0P3 pin must connect to a 1 nF capacitor for stability if it is enabled. The buffer is designed to source and sink small currents as required by the CO amplifier. The 300 mV reference and the 1.25 mV to 5mV reference cannot be enabled simultaneously.

A resistor connected in parallel with the CO sensor prevents charge from accumulating across its terminals. The output of the CO amplifier is connected to the COO pin for continuous monitoring and the AMUX for periodic sampling.

7.3.5.2 CO Connectivity Test

The built-in CO connectivity test function connects to the PREF pin and is available when the photo amplifier is not referenced to PREF. The COTEST_EN and COTEST_DIR register bits program a pull-up and pull-down switch on PREF. A 200 kΩ pull-up resistor charges the 1 µF capacitor when the CO test is not in use. When PREF is pulled low, charge is injected into the amplifier and the output pulse shape can be used to determine if the sensor is connected. An external MOSFET and pull-up resistor achieves the same function as the internal COTEST circuitry.

7.3.6 SLC Interface Transmitter and Receiver

External component selection depends on SLC protocol. Example configuration is shown

Figure 7-6. SLC Interface Circuit

In smoke detection systems where the power line carries communication signals between smoke detectors and central fire panels, the SLC interface connects to the power line to transmit and receive data from the MCU. The interface isolates the high voltage power line from the microcontroller, mitigating risk of damage and reducing external component count.

7.3.6.1 SLC Transmitter

Signals are transmitted to the power line by pulling the line low with a controlled current sink. When the driver is enabled, the microcontroller controls the SLC_TX1 and SLC_TX2 outputs by driving MCU_TX1 and MCU_TX2 high. In Figure 7-6, the SLC_TX2 output driver connects to an external transistor and current-limiting resistor. The current drawn from the power line is shown in [Equation 1](#page-26-0). The SLC_TX1 output driver is able to pull the line completely low. This configuration allows for multi-level communication.

$$
I_{SINK}\,=\frac{V_{SLC}\,-\,V_{BE}}{R_E}
$$

(1)

7.3.6.2 SLC Receiver

The SLC receiver transmits signals from the power line to the microcontroller. A reverse biased Zener diode level shifts the power line. The Zener diode is selected to drop the voltage such that when V_{LIME} is high, the SLCRX pin is above 3 V and when V_{LINE} is low, the SLCRX pin is below 0.5 V. The 100-pF capacitor filters voltage spikes that may occur on V_{LIME} . The hysteretic and deglitched comparator filters spurious noise on VLINE. The comparator output is synchronized with the 32 kHz clock before being deglitched. The hysteresis voltage and deglitch time are programmable with the SLCRX_HYS and SLCRX_DEG register bits. An internal pulldown resistor biases the Zener diode to maintain the SLC_RX voltage below 17 V, the recommended maximum.

7.3.7 AMUX

Figure 7-7. Analog Multiplexer Circuit

The AMUX switch and buffer are used to connect the various TPS8804 amplifier outputs to a single ADC. The unity-gain amplifier improves the drive strength and fidelity of the analog signals when connected to an ADC. A 330 pF to 1 nF capacitor must be connected to the AMUX pin to stabilize its output. The 10-kΩ resistor filters high-frequency noise in the analog signal. Using a 10-kΩ resistor and 1-nF capacitor reduces noise levels in the photo amplifier signal. The buffer has the option of being bypassed to remove the added offset introduced by the unity-gain amplifier. Because the AMUX requires the bias block (see Section 7.3.8), bypassing the buffer does not eliminate the AMUX current consumption.

7.3.8 Analog Bias Block and 8 MHz Oscillator

A central analog bias block connects to many of the amplifiers, drivers, and regulators. This block is enabled when any of its connected blocks are enabled. Similarly, an internal 8-MHz oscillator is enabled when the photo input amplifier is enabled. Table 7-2 lists the conditions when the bias block and 8-MHz oscillator are enabled. The bias block and 8-MHz oscillator consume current in addition to the connecting blocks whenever they are enabled. Because the specified current consumption of each block does not include the bias block or the 8-MHz oscillator, add the bias block and 8-MHz oscillator currents when calculating system power consumption. Typical values of the bias block and 8-MHz oscillator current are shown in [Section 6.6.](#page-15-0)

7.3.9 Interrupt Signal Alerts

Figure 7-8. Interrupt Signal Alert Logic

Configurable interrupt signals notify the MCU when a system anomaly occurs. The interrupt signal indicates the STATUS1 register, which has bits that latch high when reaching various condition limits such as temperature or voltage. Each of the bits in the STATUS1 register can be independently configured to send an interrupt signal by setting the MASK register bit corresponding to each STATUS1 bit. The GPIO bits must be set to 0x2 to output interrupt signals through the GPIO pin, and the STATUS_MCURX bit must be set to 1 to output interrupt signals through the MCU_RX pin. By connecting the GPIO or MCU_RX pin to the microcontroller, the MCU can be immediately notified when a STATUS1 bit changes instead of having to repeatedly read the STATUS1 register. After the device sends the interrupt signal, the signal remains high until the STATUS1 register is read, at which point the fault clears if the error condition is removed.

7.4 Device Functional Modes

7.4.1 Fault States

Figure 7-9. Fault States Diagram

The TPS8804 device uses several monitors to alert the MCU when system irregularities occur. In addition to alerting the MCU, two monitors cause the device to enter protective fault states:

- MCULDO under-voltage
- system over-temperature

The fault states reduce risk of damage and brown-outs to the system in the event of short circuits or other power errors.

7.4.1.1 MCU LDO Fault

The MCU LDO has an undervoltage monitor to notify the MCU if the LDO falls out of regulation. This monitor is enabled any time the MCU LDO is enabled and its status is in the MCU_PG register bit. A 125-μs deglitch time rejects load and line transient spikes that may briefly drop the MCU LDO voltage below the under-voltage threshold. If MCU_PG is low while the MCU LDO is enabled and it has been more than 10 ms since the LDO was enabled or changed voltage, the MCU_ERR register bit latches high. When the MCU_ERR bit is set high and the MCUERR_DIS bit is low, the MCU LDO fault state is entered.

When the MCU LDO fault state is entered, all amplifiers and drivers are disabled. The MCU LDO remains enabled to attempt to recover the system. The device enables the over-temperature monitor (OTS_EN) to prevent a VMCU short circuit from overheating the TPS8804 device. If a VMCU short circuit causes the temperature of the TPS8804 to rise, an over-temperature shutdown occurs and the MCU LDO shuts off.

There are two methods to exit the fault state. Every second in the fault state, the MCU_PG register bit is automatically read. If high, the fault state is exited. The MCU_ERR bit remains high until the STATUS1 register is read. Alternatively, if the STATUS1 register is read and MCU_PG is high, the fault state is exited. When the device exits the MCU_ERR fault state, the device re-enables all blocks that were enabled before the fault state occurred.

If an over-temperature fault occurs while in the MCU LDO fault state, the device enters the over-temperature fault state. The over-temperature fault state disables the MCU LDO in addition to the blocks that are disabled by the MCU LDO fault state. After the device exits the over-temperature fault state, it immediately re-enters the MCU LDO fault state to confirm the MCU LDO status.

7.4.1.2 Over-Temperature Fault

An over-temperature shutdown (OTS) fault occurs if OTS_EN = 1 and the die temperature exceeds 125°C. The fault is masked for 300 μs after setting OTS_EN = 1. OTS_EN must be enabled for at least 300 μs in order to determine if the die has overheated. After the device detects an over-temperature condition, it disables all drivers, amplifiers, and regulators and sets OTS_ERR to 1. This action prevents additional temperature stress caused by a short circuit.

Similar to the MCU LDO fault, the device exits the OTS fault state with two methods:

- The device checks the die temperature once every second. If the temperature is below 110°C, the device exits the fault state.
- Reading the STATUS1 register with the die temperature below 110°C exits the fault state.

When the device exits the OTS fault state, it re-enables all blocks that were enabled before the OTS fault occurred.

7.5 Programming

The TPS8804 serial interface follows the I²C industry standard. The device supports both standard and fast mode, and it supports auto-increment for fast reading and writing of sequential registers. A 33-kΩ pullup resistor connecting the SDA and SCL pins to VMCU is recommended for fast mode operation. The VMCU voltage determines the logic level for I²C communication. The CSEL pin selects the device address. When CSEL is pulled to GND, the device address is 0x3F. When CSEL is pulled to VMCU, the device address is 0x2A.

7.6 Register Maps

Table 7-3 lists the memory-mapped registers for the Device registers. All register offset addresses not listed in Table 7-3 should be considered as reserved locations and the register contents should not be modified.

Table 7-3. Device Registers

Complex bit access types are encoded to fit into small table cells. Table 7-4 shows the codes that are used for access types in this section.

Table 7-4. Device Access Type Codes

7.6.1 REVID Register (Offset = 0h) [reset = 0h]

REVID is shown in Table 7-5.

Return to [Summary Table](#page-29-0).

7.6.2 STATUS1 Register (Offset = 1h) [reset = 0h]

STATUS1 is shown in [Table 7-6](#page-31-0).

Return to [Summary Table](#page-29-0).

7.6.3 STATUS2 Register (Offset = 2h) [reset = 0h]

STATUS2 is shown in Table 7-7.

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Table 7-7. STATUS2 Register Field Descriptions

7.6.4 MASK Register (Offset = 3h) [reset = 0h]

MASK is shown in Table 7-8.

Return to [Summary Table](#page-29-0).

Table 7-8. MASK Register Field Descriptions

Table 7-8. MASK Register Field Descriptions (continued)

7.6.5 CONFIG1 Register (Offset = 4h) [reset = 20h]

CONFIG1 is shown in Table 7-9.

Return to [Summary Table](#page-29-0).

Table 7-9. CONFIG1 Register Field Descriptions

7.6.6 CONFIG2 Register (Offset = 5h) [reset = 0h]

CONFIG2 is shown in Table 7-10.

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Table 7-10. CONFIG2 Register Field Descriptions

7.6.7 ENABLE1 Register (Offset = 6h) [reset = 0h]

ENABLE1 is shown in [Table 7-11.](#page-33-0)

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Table 7-11. ENABLE1 Register Field Descriptions

7.6.8 ENABLE2 Register (Offset = 7h) [reset = 0h]

ENABLE2 is shown in Table 7-12.

Return to [Summary Table](#page-29-0).

Table 7-12. ENABLE2 Register Field Descriptions

7.6.9 CONTROL Register (Offset = 8h) [reset = 0h]

CONTROL is shown in Table 7-13.

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Table 7-13. CONTROL Register Field Descriptions

Table 7-13. CONTROL Register Field Descriptions (continued)

7.6.10 GPIO_AMUX Register (Offset = Bh) [reset = 0h]

GPIO_AMUX is shown in Table 7-14.

Return to [Summary Table](#page-29-0).

7.6.11 COSW Register (Offset = Ch) [reset = 0h]

COSW is shown in Table 7-15.

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Table 7-15. COSW Register Field Descriptions

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Table 7-15. COSW Register Field Descriptions (continued)

7.6.12 CO Register (Offset = Dh) [reset = 0h]

CO is shown in Table 7-16.

Return to [Summary Table](#page-29-0).

Table 7-16. CO Register Field Descriptions

7.6.13 LEDLDO Register (Offset = Fh) [reset = 0h]

LEDLDO is shown in Table 7-17.

Return to [Summary Table](#page-29-0).

Table 7-17. LEDLDO Register Field Descriptions

Table 7-17. LEDLDO Register Field Descriptions (continued)

7.6.14 PH_CTRL Register (Offset = 10h) [reset = 0h]

PH_CTRL is shown in Table 7-18.

Return to [Summary Table](#page-29-0).

Table 7-18. PH_CTRL Register Field Descriptions

7.6.15 LED_DAC_A Register (Offset = 11h) [reset = 0h]

LED_DAC_A is shown in Table 7-19.

Return to [Summary Table](#page-29-0).

Table 7-19. LED_DAC_A Register Field Descriptions

7.6.16 LED_DAC_B Register (Offset = 12h) [reset = 0h]

LED_DAC_B is shown in [Table 7-20.](#page-37-0)

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Table 7-20. LED_DAC_B Register Field Descriptions

8 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

The TPS8804 supports a variety of smoke alarm platforms, including single-wave or dual-wave photoelectric smoke and CO detection.

8.2 Typical Application

Figure 8-1. Dual-Wave Photoelectric Smoke and CO Detector

8.2.1 Design Requirements

In this example, a smoke alarm requires the following:

- 100 MΩ photoamplifier transconductance with sub-nanoamp detection
- 100 mA IR LED current with 1-mA/°C temperature compensation
- 50mA blue LED current with 0.1mA/°C temperature compensation

8.2.2 Detailed Design Procedure

8.2.2.1 Photo Amplifier Component Selection

To meet the 100-MΩ photoamplifier transconductance requirement, set the gain stage to 35x with PGAIN = 11. Because the application requires sub-nanoamp current detection, reference the photo amplifier to PREF and set PREF SEL = 1. This reference offsets the input stage output by 50 mV and offsets the gain stage output by 225 mV. Because the application uses PREF, the gain stage amplification reduces to 32.25x. Divide 100 M Ω by 32.25x to get 3.1 MΩ. The gain is distributed across two resistors, therefore use a resistor with a value of approximately 1.55 MΩ. A 1.5-MΩ resistor is selected. The achieved transconductance is 96.8 MΩ. Use 10-pF of compensation capacitance in parallel with the 1.5-MΩ resistors. Use an oscilloscope with averaging to verify the photo amplifier is quickly settling but not overshooting. If the photo amplifier has overshoot, increase the compensation capacitance. If the photo amplifier is settling slowly, decrease the compensation capacitance.

8.2.2.2 LED Driver Component Selection

The LED current depends on the TEMPCO bits, PDAC register and CSA and CSB resistors. Changing any of these values affects the LED current and temperature compensation. The following method selects the TEMPCO, PDAC, and CSA resistor value based on the required LED current and temperature compensation. The 100-mA LED current and 1 mA/°C temperature compensation is used as an example for LED A. Repeat the process for LED B.

- 1. Determine the room temperature current and temperature compensation required by the application.
	- 100mA and 1mA/°C is required by the design.
- 2. Calculate the compensation in percentage per degree by dividing the compensation coefficient by the current and multiplying by 100.
	- 1 mA/°C divided by 100 mA is 1%/°C.
- 3. Use [Table 8-1](#page-40-0) or [Table 8-2](#page-40-0) to select a TEMPCO setting which contains the required compensation. If the required compensation is in two ranges, use the range with a higher TEMPCO setting. If the required temperature coefficient is not in any of the ranges, choose the TEMPCO and PDAC setting closest to the required temperature coefficient, then go to step 5.
	- 1%/°C is between the mimumum and maximum for TEMPCO = 11.
- 4. Calculate the target CSA voltage. Divide the driver temperature coefficient [mV/°C] by the desired temperature coefficient [%/°C] and multiply by 100.
	- 1.040 mV/°C divided by 1 %/°C is 104 mV.
- 5. Calculate the CSA resistor by dividing the target CSA voltage by the required current and subtracting 0.1 Ω for internal resistance.
	- 104 mV divided by 100 mA is 1.04 Ω . Subtract 0.1 Ω to get 0.94 Ω .
- 6. Select the closest available resistor and calculate the final CSA voltage by multiplying the required current by the total resistance (external and internal).
	- Use a 0.92 Ω resistor. Multiply 100 mA and 1.02 Ω to get 102mV CSA voltage.
- 7. Calculate the PDAC value by subtracting the final CSA voltage by the specified CSA voltage at PDAC = 0x00 and dividing the result by 1.176 mV (the DAC LSB, equal to 300 mV divided by 255).
	- 102 mV minus 79 mV is 23 mV, divided by 1.176 mV is 20. Write 0x14 to the PDAC register.
- 8. Calibrate the PDAC value. If using the LED A driver, read the CSA_BIN register bits and add 0x11 if CSA_BIN=00b, add 0x06 if CSA_BIN=01b, subtract 0x06 if CSA_BIN=10b, or subtract 0x11 if CSA_BIN=11b. The CSA_BIN value varies from unit to unit and must be read on each unit calibrated using this method. Alternatively, measure the CSA or CSB voltage using the MCU ADC and adjust PDAC accordingly.
	- The microcontroller reads that a unit has CSA_BIN=01b. 0x20 is written to PDAC_A.

Table 8-1. Temperature Coefficients for Each TEMPCOA and DAC_A Setting

Use the same procedure for the blue LED, requiring 50 mA and 0.1 mA/°C, to calculate TEMPCOB = 10, RCSB $= 6.8$ Ω, VCSB = 345 mV, PDAC_B = 0x85 (before calibration).

The two drivers are identical, except for the CSA_BIN code to improve the accuracy of the LED_A driver for IR LEDs. Connect the IR LED to the LED A driver and the blue LED to the LED B driver in multi-wave systems.

8.2.2.3 LED Voltage Supply Selection

Each of the LED anodes must have enough voltage to forward bias the LED, regulate the CSA and CSB voltage, and exceed the driver dropout voltage requirement from DINA to CSA and DINB to CSB. A typical IR LED at 100 mA has 1.5-V forward voltage. The LED driver dropout voltage at 100 mA is 300 mV. With the CSA voltage set to 100 mV, the dropout voltage of 300 mV, and forward voltage of 1.5 V, at least 1.9 V must be applied to the IR LED anode for current regulation. Connect the IR LED anode to LEDLDO and set LEDLDO_EN = 1 to charge the IR LED anode capacitor.

A typical blue LED at 50 mA has 4 V forward voltage. For the blue LED, the CSB voltage is 340 mV, the dropout voltage is 300 mV, and the forward voltage is 4 V. Supply over 4.64 V to the anode for the duration of the LED pulse. With a 47 µF capacitor derated to 30 µF, 100 µs LED pulse, the anode voltage drops by 170 mV.

Thus, the capacitor must be charged to 4.81 V. If the VCC voltage is between 5 V and 6 V, connect the blue LED anode to VCC through a 1-kΩ resistor. If VCC is between 6 V and 15 V, connect the blue LED anode to LEDLDO and set LEDLDO EN = 1 to charge the blue LED anode capacitor. The LED LDO has a diode voltage drop between the VSLC voltage and LEDLDO voltage. The LEDLDO prevents the DINA pin from exceeding its recommended operating limit of 11.5 V.

8.2.2.4 Regulator Component Selection

To stabilize the output voltage on each regulator, install 1-µF capacitors on VINT, VMCU, and PLDO. Connect the MCUSEL pin to GND to set the MCU LDO voltage to 1.8V. The MCU LDO can be set to other voltages by changing the MCUSEL pin connection. Connect the MCUSEL pin to GND through a 1 nF capacitor to set the MCU LDO voltage to 3.3 V. Connect MCUSEL to VINT to set the MCU LDO to 2.5 V. Connect MCUSEL to GND with a 620-Ω resistor to set the MCU LDO to 1.5 V.

8.2.3 Application Curves

All curves use the schematics shown in [Figure 8-1](#page-38-0). The photo amplifier curves do not have the 470 kΩ PREF resistor installed.

9 Power Supply Recommendations

A 4.5-V to 15-V power supply is recommended on VCC and VSLC. If a blue LED is used with the LED driver, higher voltage may be required. Ensure the power supply can tolerate transient currents caused by the LED driver. A supply capable of 5 mA average current is generally sufficient. Ensure the power supply's rise time is less than 100 ms.

10 Layout 10.1 Layout Guidelines

These blocks require careful layout placement:

- Photo amplifier
- CO amplifier
- Ground plane and traces

10.1.1 Photo Amplifier Layout

The photo amplifier is a very sensitive analog block in the TPS8804 device. Minimal trace lengths must be used to connect the photodiode and relevant external components to PDP, PDN, PDO, PREF and AGND. It is recommended to shield the PDP, PDN, PDO, and PREF traces with the AGND plane.

10.1.2 CO Amplifier Layout

Similar to the photo amplifier, the CO amplifier is very sensitive to noise. Connect the CO electrochemical sensor close to the TPS8804 device and shield the COP, CON, and COO traces with the AGND plane.

10.1.3 Ground Plane Layout

Connect AGND and DGND to the ground plane. Ensure there is a short path from AGND to DGND. Route PGND and its associated blocks (LED driver, SLC transmitter) separately from the ground plane. Connect PGND to AGND at a single point near the IC.

10.2 Layout Example

Figure 10-1. Photo Amplifier Layout

[TPS8804](https://www.ti.com/product/TPS8804) [SLVSF29C](https://www.ti.com/lit/pdf/SLVSF29) – OCTOBER 2019 – REVISED AUGUST 2021

Figure 10-2. CO Amplifier Layout

Figure 10-3. Ground Layout

11 Device and Documentation Support

11.1 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com.](https://www.ti.com) Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

11.2 Support Resources

TI E2E™ [support forums](https://e2e.ti.com) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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11.3 Trademarks

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11.4 Electrostatic Discharge Caution

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

11.5 Glossary

[TI Glossary](https://www.ti.com/lit/pdf/SLYZ022) This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

www.ti.com 9-Aug-2022

PACKAGE MATERIALS INFORMATION

*All dimensions are nominal

GENERIC PACKAGE VIEW

DCP 38 PowerPAD TSSOP - 1.2 mm max height

4.4 x 9.7, 0.5 mm pitch SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

PACKAGE OUTLINE

DCP0038A PowerPAD[™] TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. Reference JEDEC registration MO-153.
- 5. Features may differ or may not be present.

EXAMPLE BOARD LAYOUT

DCP0038A PowerPAD™ TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.
- 10. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

DCP0038A PowerPAD™ TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

12. Board assembly site may have different recommendations for stencil design.

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